

Effect of Different Calcination Process and Gd₂O₃ as Impurities on the Different Phases of Bi-Based Superconductor

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ABSTRACT

In this research two samples of a nominal composition $Bi_{1.6}Pb_{0.4}Sr_2Ca_2Cu_3O_x$ were prepared by the solid state reaction method, using two different routes. Codes A and B are used to refer to the two samples. In preparing sample A, the standard method for calcination was used, while for sample B, the $SrCO_3$ and $CaCO_3$ were calcinated at $1100^{\circ}C$ for 3 h. Calcination was done separately on $SrCO_3$ and $CaCO_3$ in order to eliminate CO_2 . Then after mixing and grinding, the powder mixtures of Bi_2O_3 , CuO, PbO, SrO and CaO were calcinated at $840^{\circ}C$ for 70 h. Also, the samples (samples C) of nominal compositions $Bi_{1.6}Pb_{0.4}Sr_2Ca_2Cu_3O_x + \% x Gd_2O_3$ (% x = 0, 3, 5, 7 and 9) have been synthesized by this method. The XRD and SEM results show that addition of Gd_2O_3 helps to increase the amount of Bi-2212 phase, while alternative calcination process improves the formation of the Bi-2223 phase. In addition, the AC susceptibility measurements confirm the XRD and SEM results.

Keywords: Bi-Pb-Sr-Ca-Cu-O System; X-Ray Diffraction; Scanning Electron Microscopy; AC Susceptibility

1. Introduction

The Bi-Pb-Sr-Ca-Cu-O system exhibits three different superconducting phases of (Bi-Pb)₂Sr₂CuO_x (Bi-2201), (Bi-Pb)₂Sr₂CaCu₂O_x (Bi-2212) and (Bi-Pb)₂Sr₂Ca₂Cu₃O_x (Bi-2223), which show critical temperatures (T_c) of about 10, 80 and 110 K, respectively [1-3]. In the BSCCO system, the Bi-2212 phase is thermodynamically stable over a wide temperature range and among the three members of the BSCCO family the Bi-2212 and Bi-2223 phases have been the most extensively studied to date. In contrast to the Bi-2212 phase, the Bi-2223 phase is stable only in an extremely narrow temperature range and thus it is difficult to prepare single phase Bi-2223 ceramics [4]. Usually, in polycrystalline Bi-based superconducting preparations, these two phases tend to co-exist. The calcination process used in this research for Bi-based materials helps to increase the amount of the Bi-2223 phase relative to the amount of the Bi-2212 phase.

Effect of rare earth and some oxide as impurities or substitution of them for Bi and Sr in polycrystalline Bi-based superconductor's properties such as T_c and J_c have been investigated by several researchers [5-15]. Here we have studied the effect of Gd_2O_3 as impurities on the

general formula of $Bi_{1.6}Pb_{0.4}Sr_2Ca_2Cu_3O_x + Gd_2O_3$ composites and investigated the addition of these impurities on different phases of Bi-Based superconductor.

2. Experimental

2.1. Different Calcination Process

In the usual solid state reaction method for producing Bi-based superconductors, calcination stage is used to eliminate the carbonates and to produce an oxide with a nominal composition (Bi-Pb)₂Sr₂Ca_{n-1}Cu_nO_x [7]. Calcination of powder mixtures of Bi₂O₃, CuO, PbO, SrCO₃ and CaCO₃ is performed at temperatures less than or equal to 900°C. The decomposition temperatures for CaCO₃ and SrCO₃ are 900°C and 1290°C, respectively [16]. Therefore, elimination of CO₂, at 850°C, from this mixture, can take a long time; but if the calcination temperature is increased, the mixture could melt.

In this research, two samples of nominal compositions Bi_{1.6}Pb_{0.4}Sr₂Ca₂Cu₃O_x were prepared by the standard solid-state reaction method and by using two different routes. Codes A and B are used to refer to the samples. In preparing sample A, the oxide powders (Bi₂O₃, PbO, SrCO₃, CaCO₃ and CuO), taken in stoichiometric proportions, were ground and calcinated at 840°C for 70 h. The powders

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were well mixed and ground in an agate mortar and pestle and pressed into pellets (15 mm in diameter and 2 mm in thickness) and sintered at 850°C for 230 h with four intermediate grinding processes. The chosen rate of temperature increase and decrease was 2°C-min⁻¹. For sample B, the SrCO₃ and CaCO₃ were calcinated at 1100°C for 3 h. The calcination was done in order to eliminate CO₂ separately for SrCO₃ and CaCO₃. Then after mixing and grinding, the powder mixtures of Bi₂O₃, CuO, PbO, SrO and CaO were calcined at 840°C for 70 h. The conditions for the second stage of calcination and sintering were similar to those for sample A.

The amount of residual of CO₂ can be measured by the LOI (loss on ignition) coefficient. Loss on ignition is a test used in inorganic analytical chemistry, particularly in the analysis of minerals. It consists of strongly heating (igniting) a sample of the material at a specified temperature, allowing volatile substances to escape until its mass ceases to change. The process may be repeated to show that mass-change is complete. LOI is defined as [17]:

$$LOI = \frac{W - W'}{W}$$

where W and W' are the weight of the sample before heat treatment and the weight of the sample after heat treatment, respectively. Hence

$$xSrCO_3 \quad \underline{\text{heat treat}} \quad xSrO + xCO_2$$

$$LOI(SrCO_3) = \frac{xSrCO_3 - xSrO}{xSrCO_3} = \frac{xCO_2}{xSrCO_3}$$

$$LOI(SrCO_3) = \frac{44.0095}{147.6289} = 0.2981$$

and

$$x$$
CaCO₃ heat treat x CaO + x CO₂
LOI(CaCO₃) = $\frac{44.0095}{100.0865}$ = 0.4397

where *x* in the above equations is used to denote the mol number of the indicated materials and the coefficient LOI is constant for each desired amount of the composition. The samples A and B are compared to determine the effect of further calcination stage in B sample on the formation of the Bi-2223 phase.

2.2. Addition of Gd₂O₃ as Impurities

• The Bi_{1.6}Pb_{0.4}Sr₂Ca₂Cu₃O_x + % x Gd₂O₃ (% x = 0, 3, 5, 7 and 9) composites were papered by two steps. First, the (Bi-Pb)₂Sr₂Ca₂Cu₃O_x was synthesized by conventional solid-state reaction method. High purity (99.5%), Bi₂O₃, PbO, SrCO₃, CaCO₃ and CuO powders were mixed in the appropriate stoichiometric ratio and grind-

- ing in an agate mortar. The well-mixed powders were calcined at 840° C for 70 h. Finally, after regrinding the $(Bi-Pb)_2Sr_2Ca_2Cu_3O_x$ and Gd_2O_3 powders, the appropriate amounts of these powders were mixed and a homogenous powders were pressed in pellets and sintered at 850° C for 230 h. Sample codes (C_{000} , C_{003} , C_{005} , C_{007} and C_{009}) are used to refer to the samples.
- The X-ray diffraction (XRD) studies were preformed with Cu-Kα radiation. The surface morphology of samples, which is an important surface property and very useful for understanding their defect structure, grain size, voids, etc., was studied by scanning electron microscopy (SEM). Finally, cylindrical specimens were cut from the sintered samples and used for AC susceptibility measurements. The real part of the AC susceptibility was measured with a Lake Shore Model 7000 AC susceptometer. The measurements were performed at a frequency of 333.3 Hz as a function of temperature at fixed AC magnetic field amplitude of 500 A/m. The AC field was applied parallel to the cylindrical axis.

3. Results and Discussions

3.1. Effect of Different Calcination Process

3.1.1. X-Ray Diffraction

Figure 1 shows the indexed X-ray diffraction patterns for samples A and B. The majority of the diffraction lines correspond mainly to Bi-2223 and Bi-2212 and the unit cells are orthorhombic for both samples. Due to the coexistence of Bi-2212 phase with Bi-2223 phase, a quantitative analysis is often required to estimate the amount of Bi-2212 and Bi-2223. XRD is the most widely used method for this kind of quantitative phase analysis. The volume fraction of Bi-2223 and Bi-2212 phases can be estimated using various methods. Some workers [18-20] have used (002) and (115) or (0010) and (008) peaks of Bi-2223 and Bi-2212 phases, respectively, and others [21] used all the peaks of the Bi-2223 and Bi-2212 phases for the estimation of the volume fraction. Here the (0010) and (008) peaks of Bi-2223 and Bi-2212 phases are used to estimate the volume fraction of the phases present. The fractional amount of the Bi-2223 phase relative to the Bi-2212 phase could be estimated from the intensities according to:

Bi-2223% =
$$\frac{I(0010)}{I(0010) + I(008)}$$

Bi-2212% =
$$\frac{I(008)}{I(0010) + I(008)}$$

where I is the intensity of peaks corresponding to the phases present. The volume fractions of the Bi-2223 and Bi-2212 in sample B are 40% and 31%; in sample A the

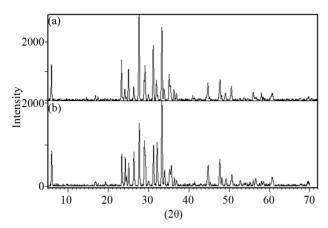


Figure 1. XRD patterns for samples A and B after the final stage of the heat treatment.

corresponding volume fractions are 21% and 39%, respectively. This shows that further calcination favors the formation of Bi-2223 phase.

3.1.2. SEM Studies

The scanning electron micrographs of the samples after the final sintering step are shown in Figures 2(a) and (b). It is clear from these figures that the superconducting grains seem to be connected with each other while there are some unfilled spaces among them. The grain size and the distribution of grains on the surface of the samples are quite different. The surface of sample A is smoother and denser, while that of sample B has larger grains and more voids. Khalil [22,23] reported that the decrease of porosity might be related to an increase in (a) grain coupling strength and (b) degree of grain orientation of the BSCCO samples. On the other hand, Tampieri et al. [24] reported that the Bi-2212 phase has higher crystallographic density and stronger intergranular links than the Bi-2223 phase. Characteristic flaky grains of (Bi,Pb)-2212 and plate-like grains which are the typical grain structure of (Bi,Pb)-2223 are visible in both samples. Here the layered structure is only partially maintained with reduction in grain size and texture. In the XRD patterns of the samples, it is seen that sample B contains more Bi-2223 phase than sample A. Therefore, the highest density value would be expected for sample A. Here, the grains become more compressed and closely packed leaving a large number of inter-grain voids. These results agree with those obtained by XRD. The average grain size at different spots of the samples is between 1 and 9 µm. The size of the largest particle in sample B is almost twice as large as in sample A.

3.1.3. AC Susceptibility Studies

Positioning For the superconducting samples, the real part of the AC susceptibility $\chi'(T)$ was measured after the final sintering step. The real part of the AC susceptibility

versus temperature for samples A and B is shown in **Figure 3**. The superconducting transition temperature was determined from the onset of the diamagnetic signal. The diamagnetic transition in the real part of the AC susceptibility occurs sharply at T_c (onset). The onset temperature of both samples lies between 108 and 110 ± 1 K. Curves A and B show that initially both phases of Bi-2223 and Bi-2212 are present in the samples. The sharper transition observed in sample B suggests that this sample present a higher superconducting fraction of 2223 than sample A. But the actual estimate of superconducting volume fraction is not possible by this experiment [5,11].

3.2. Effect of Gd₂O₃ as Impurities

3.2.1. X-Ray Diffraction

Figure 4 shows the X-ray diffraction patterns for C_{000} , C_{003} , C_{005} , C_{007} and C_{009} samples. The Bi-2223 and Bi-2212 phases co-exist in the composites. The majority of the diffraction lines correspond mainly to Bi-2223 and Bi-2212 and the unit cells are orthorhombic for all samples. The fraction amount of the Bi-2223 phase relative to the Bi-2212 phase were estimated from the intensities as Section 3.1.1:

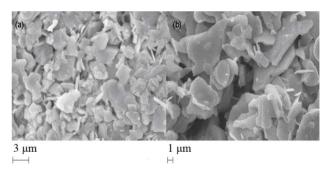


Figure 2. SEM photograph for (a) A sample; and (b) B sample.

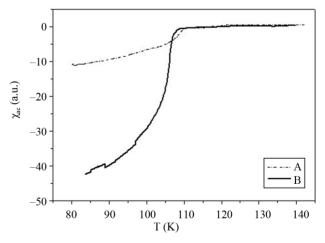


Figure 3. Temperature dependence of the real part of the AC susceptibility of the A and B samples.

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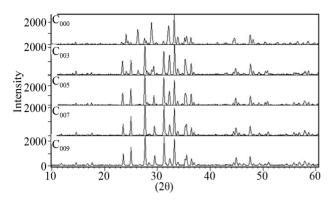


Figure 4. XRD patterns of C_{000} , C_{003} , C_{005} , C_{007} and C_{009} samples after the final stage of the heat treatment.

3.2.2. SEM Studies

The scanning electron micrographs of the samples after the final sintering step are shown in **Figures 5(a)-(d)**. It is clear from the figures that the superconducting grains seem to be connected with each other, while there are some unfilled spaces among them. The grain size and the distribution of grains on the surface of the samples are quite different. Again here characteristic flaky grains of (Bi,Pb)-2212 and plate-like grains which are the typical grain structure of (Bi,Pb)-2223 are visible in these samples. The surface of the C_{007} sample is smoother and denser, while C_{003} and C_{005} samples have larger grain sizes and more voids. In the XRD pattern of the samples, it is seen that the superconducting phases Bi-(2212) increase as the wt% of Gd_2O_3 increases. Therefore, the highest density value would be expected for the C_{009} sample.

3.2.3. AC Susceptibility Studies

For the superconducting samples, the real part of the AC susceptibility $\chi'(T)$ was measured after the final sintering step. The real part of the AC susceptibility versus temperature for samples C_{000} , C_{003} and C_{007} is shown in **Figure 6**. The onset temperature of samples C_{000} , C_{003} and C_{007} are 112, 109, 105 \pm 1 K respectively. The C_{000} and C₀₀₃ curves show that initially two phases Bi-2223 and Bi-2212 are present in these samples. In the C_{000} sample, the transition of $\chi'(T)$ for the intragranular component is sharper. In the C_{007} sample, there is a weak transition in 105 K that shows phase Bi-2223 approximately has been destroyed. Phase Bi-2223 decreases by increasing the wt% of Gd₂O₃ but the actual estimate of superconducting volume fraction is not possible by this experiment. For C_{005} and C_{009} Samples, the $\chi'(T)$ behaviors are mostly the same of C_{003} and C_{007} samples respectively.

4. Conclusion

The X-ray diffraction studies in room temperature show that there are two major phases of Bi-2223 and Bi-2212 in the diffraction patterns. The orthorhombic structure

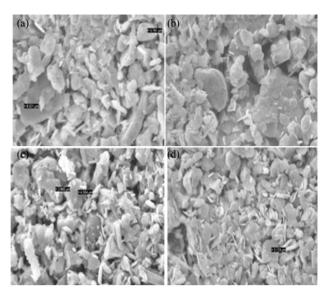


Figure 5. SEM photograph for samples (a) C_{003} ; (b) C_{005} ; (c) C_{007} ; and (d) C_{009} .

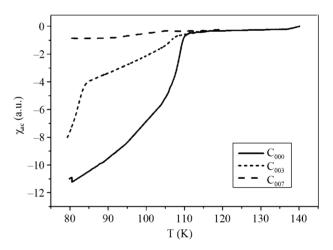


Figure 6. The temperature dependence of the real part of AC susceptibility for the $C_{000},\,C_{003}$ and C_{007} samples.

was observed for all samples. The XRD and SEM results show that G_2O_3 admixture helps to increase the amount of 2212 phase. Also, these results show that an alternative calcination favors the formation of the Bi-2223 phase and the size of the largest particle is increased. The AC susceptibility studies show that the onset temperature of samples A_{000} , A_{003} and A_{007} are 112, 109, 105 \pm 1 K respectively and new calcination process improves the formation of the Bi-2223 phase.

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