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**Numerical Investigation of Contact Angle Effect on Counter-Current Spontaneous Imbibition**

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has been presented as "Poster" in

The First International Conference on Improved/Enhanced Oil and Gas Recovery,  
April 22-24, 2017, Tehran, Iran.

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Conference Chair





# Numerical Investigation of Contact Angle Effect on Counter-Current Spontaneous Imbibition

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## Abstract

Medium wettability plays the main role during spontaneous imbibition (SI) in fractured porous media; however, one can rarely find pore-scale studies addressing wettability effects on this process. In present work Cahn–Hilliard phase field coupled with Navier–Stokes equations were solved using finite element method to simulate counter-current SI in a horizontal heterogeneous porous medium containing fracture. Capillary governed fluid displacement in media with different contact angles -  $\theta=\pi/10$  (extremely water-wet) up to  $\theta=\pi/2$  (neutral wet) - were simulated. The simulated models realistically captured micro-scale mechanisms during imbibition process in strongly water wet media, e.g., oil film thinning and rupture, fluids' contact line movement, water bridging and oil drop detachment. Water capillary fingering through matrix and oil drop expulsion from matrix grains to the fracture were evident displacement phenomena in strongly water wet media. There was a specific grain contact angle,  $\theta=\pi/4$ , above it matrix oil recovery was negligible and below it the imbibition rate and oil recovery were significantly increased by decreasing contact angle. For instance, after 5 s, almost 20% of the matrix oil was recovered in the model with  $\theta=\pi/10$ , while final recovery of the models with  $\theta>\pi/4$  was less than 10% even after more than 1 min.

**Keywords:** Counter-current imbibition; Phase-field method; Wettability; Fractured porous media

Gunde et al. (2013) observed that water tends to imbibe through smaller pores and oil phase expellees from the relatively larger pores. They also concluded that relative permeability of wetting phase increases by contact angle. However, LBM demonstrated some limitations for immiscible displacements especially at high viscosity ratios.

In this paper, PFM coupled with Navier–Stokes equation was employed to simulate two-phase flow during counter-current SI in a fractured porous medium. Finite element method was used to solve the equations with proper boundary conditions in a robust software, COMSOL multiphysics.

## Result & discussion

Capillary forces imbibe water into the porous matrix, however viscous forces cause water flow in the fracture and the balance between them determines microscopic distribution of fluids in pore-spaces. Through invasion of wetting phase into the porous medium, oil droplets are expelled one by one to the fracture, in good agreement with experimental observations. Figure 1 shows concentration, pressure and velocity distribution profiles at  $t = 20$  s for the simulated model. Pressure profile in Figure 1 b reveals that the middle finger has a lower pressure compared to the other ones, hence has lower chance to overcome oil bank resistance.

The stabilized distribution of water and oil (blue and red phases, respectively) in the models with different contact angles are shown in Figure 2. In neutral wet condition ( $\theta=\pi/2$ ), oil droplet expulsion does not occur and water-oil interface just moves a little bit toward the matrix (Figure 2a). In the cases of  $\theta=\pi/3$  and  $\theta=\pi/4$ , few oil blobs are expelled from matrix's top-right and middle, however water imbibition takes place just through small parts of porous medium, very close to the fracture (Figure 2b and c).

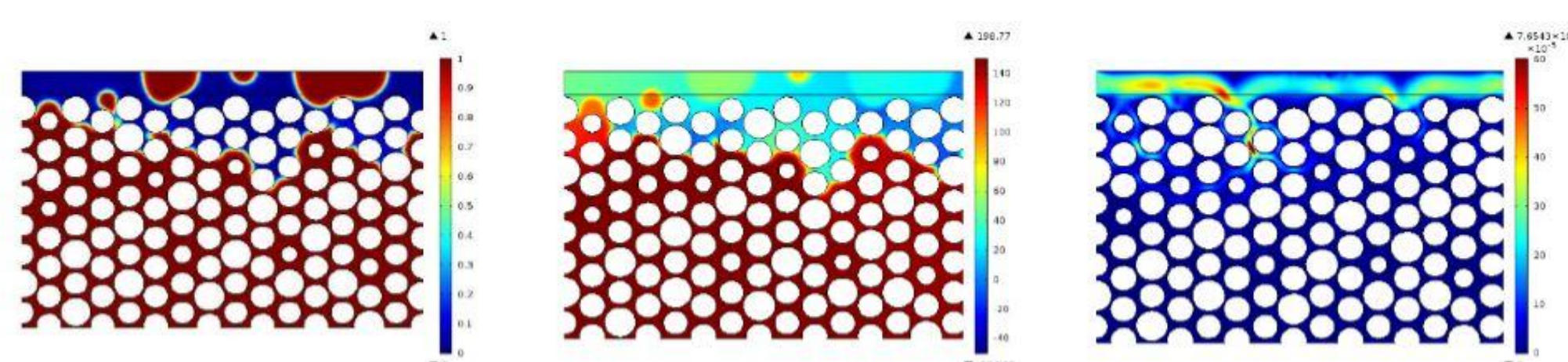


Fig. 1. (a) concentration (b) pressure (Pa) and (c) velocity (m/s) distribution profiles at  $t = 20$  s for the simulated.

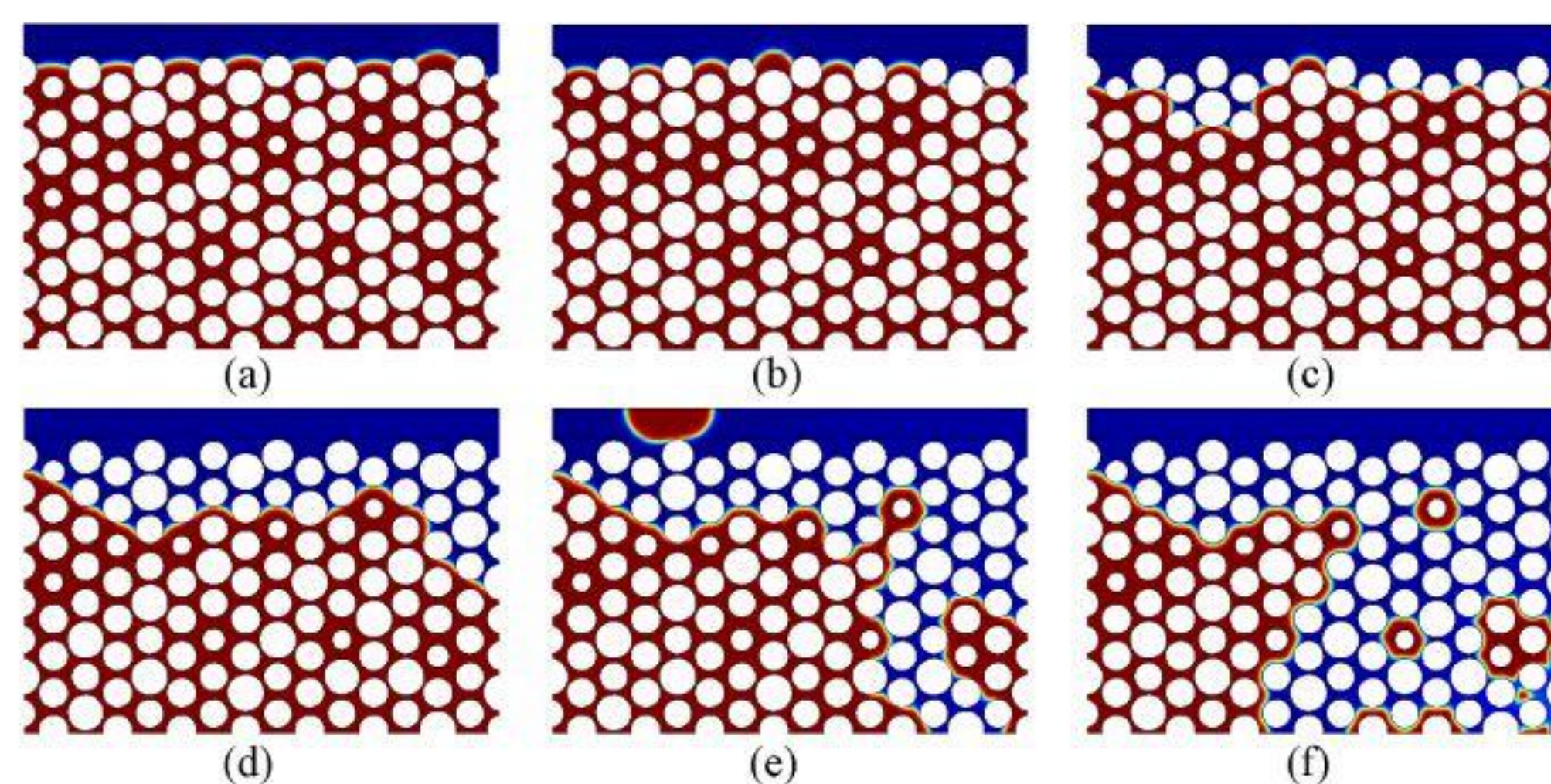


Fig.2. Snapshots of stabilized fluid distributions for the simulated model with different grain contact angles of. (a)  $\theta = \pi/2$ , (b)  $\theta = \pi/3$ , (c)  $\theta = \pi/4$ , (d)  $\theta = \pi/6$ , (e)  $\theta = \pi/8$ , and (f)  $\theta = \pi/10$ .

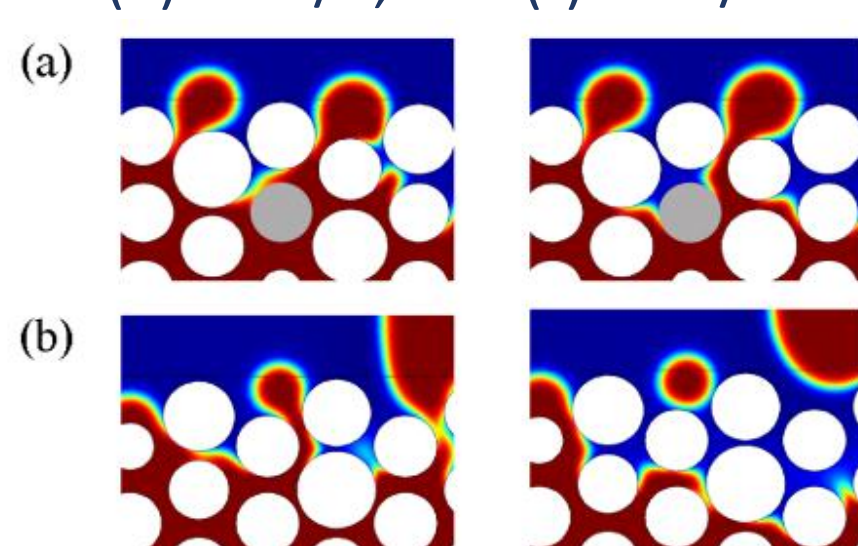


Fig.3. Two enlarged sections of the simulated model with  $\theta=\pi/8$  at two successive instants during imbibition process.

Water imbibed zone becomes considerable as  $\theta$  decreases to  $\pi/6$  (Figure 2d), in which water phase forms a front with a regular shape, without any recognizable finger. When the medium is extremely water-wet,  $\theta=\pi/8$  and  $\pi/10$  (Figure 2e and f) water capillary fingers propagate deeply into the matrix and some oil droplets with different sizes are trapped in various parts of the porous medium. Figure 3 shows two enlarged sections of the simulated medium at two instants during described water imbibition process (with  $\theta=\pi/8$ ). As demonstrated in Figure 3a, as water front approaches the marked grain, the film of oil phase on the grain surface narrows until it ruptures; hence water phase contacts the grain's surface. Thereafter, water–oil contact line movement takes place on the grain surface during water invasion process, until water phase surrounds the whole grain. Figure 3b shows how detachments of two oil drops (with different sizes) occur as a result of bridging of water films between adjacent grains and hence oil film thinning and rupture.

## Conclusions

The aim of the present work was to assess the effect of medium wettability on the water-oil displacement during matrix-fracture interaction in the process known as counter-current spontaneous imbibition (SI). Different pore-scale mechanisms such as oil film thinning and rupture, fluids' contact line movement, water bridging and oil drop detachment were captured in strongly water wet condition (i.e.,  $\theta=\pi/8$ ). It was found that fluid distributions are strongly dependent on the matrix wettability and there is a specific grain contact angle,  $\theta=\pi/4$ , above it matrix oil recovery reduces drastically. In addition, the obtained results showed that phase field method is able to capture successfully pore level mechanisms in counter current SI.

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