



# The effect of cobalt-doping on microstructure and dielectric properties of $\text{CaCu}_3\text{Ti}_4\text{O}_{12}$ ceramics



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## ABSTRACT

Ceramics of  $\text{CaCu}_{3-x}\text{Co}_x\text{Ti}_4\text{O}_{12}$  (CCCTO,  $x = 0, 0.2, 0.4$  and  $0.6$ ), with cubic lattice structure, were fabricated using a semi-wet method. The dielectric properties of the prepared samples were studied at 1 kHz frequency in the temperature range of 300–600 K, as well as in the frequency range of 50 Hz–200 kHz at room temperature. The results showed that the dielectric constants of the as-prepared samples in the frequency range of 50 Hz–200 kHz, at room temperature, are reasonably high ( $1.7 \times 10^4 \leq \epsilon \leq 6 \times 10^4$ ). It was also found out that the dielectric loss ( $\tan\delta$ ) of the prepared samples decreased by increasing the cobalt concentration at low and middle frequencies. The dielectric loss decreased from 0.87 for an undoped sample  $\text{CaCu}_3\text{Ti}_4\text{O}_{12}$  (CCTO), to 0.15 for a doped sample (CCCTO) with  $x = 0.6$ , at 50 Hz frequency. However, the dielectric constant ( $\epsilon$ ) values for the samples doped with cobalt were found to be higher than that of for the undoped sample. Moreover, the XRD patterns as well as the SEM images and EDX results revealed that the Cu-rich phase (CuO) decreased at the CCTO grain boundaries, while at the same time  $\text{Co}_2\text{TiO}_4$  and  $\text{CaTiO}_3$  phases with good dielectric insulating behavior having been formed at the boundaries. This causes the increase of the resistance at the grain boundaries leading to lower leakage current which in turn results in a decrease of the dielectric loss. These results were confirmed by using the impedance spectroscopy analysis. Our results indicate that the cobalt doped CCTO ceramics can be suggested as good candidates to be used in fabricating microelectronic and memory devices with high dielectric constant and low dielectric loss.

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## 1. Introduction

In the last two decades, calcium copper titanate (CCTO), due to its giant dielectric constant ( $>10^4$ ) as well as good thermal and frequency stability, in the temperature range of 100–600 K and frequencies up to  $10^6$  Hz, has attracted much attention in a variety of applications such as fabricating microelectronic and memory devices [1–3]. However, the thermal independence of the CCTO dielectric constant has not been seen in ferroelectric materials, which makes the ferroelectric materials unsuitable to be used for various applications [2]. Theoretical studies have shown that CCTO can have a dielectric constant of about 40–50 [2,4,5], while the

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obtained experimental values are extremely higher. In other words, this high dielectric constant has roots in the extrinsic nature of CCTO ceramics. It has been suggested that this behavior corresponds to the microstructure of these ceramics, in which in their structure semiconducting grains are surrounded by CuO phase [1,6]. It has also been reported that the presence of an internal barrier layer capacitance (IBLC), at  $T > 100$  K, is responsible for the giant dielectric constant in CCTO ceramics [7,8]. This phenomenon is associated with Maxwell-Wagner mechanism, which is the main characteristic of the electric materials having non-homogenous structures [9]. In addition, the impedance spectroscopy results of CCTO ceramics have revealed that there is a big difference between the resistance of the grains and the grain boundaries. This big difference in the resistance results in the formation of a large internal barrier and therefore increases the CCTO dielectric constant [5]. Another important parameter regarding the dielectric properties of

CCTO is the dielectric loss ( $\tan\delta$ ), which is directly related to the conductivity of the grain boundaries [10–12]. The impedance spectroscopy analysis has confirmed the relation between the dielectric loss ( $\tan\delta$ ) and the conductivity at the grain boundaries, in CCTO ceramics. The increase of the conductivity at the grain boundaries causes the increase of the leakage current which in turn results in a higher dielectric loss [13]. Many attempts have been made to reduce the dielectric loss in CCTO ceramics, since the high  $\tan\delta$  makes it less appropriate to be used in microelectronic devices [14]. The greatest tendencies for decreasing  $\tan\delta$  have been found to be along with the reduction in the dielectric constant [13,15–21]. In CCTO ceramics, the content of Cu has a significant influence on its dielectric properties [22]. Chun-Hong Mu et al. [13] have doped  $\text{Sr}^{2+}$  at  $\text{Cu}^{2+}$  site in the CCTO ceramic. Their results showed changes in the grain boundaries structure caused a reduction in the dielectric loss as well as a decrease in the dielectric constant to less than  $10^4$ . Yueyue Yan et al. [15] have reported that adding  $\text{CaTiO}_3$  into CCTO ceramic and its congregation at the boundaries reduced the  $\tan\delta$  along with the decrease in the dielectric constant to the values less than 5000. According to these studies, it seems to be possible to decrease the dielectric loss ( $\tan\delta$ ) by controlling the structure and chemistry of the grain boundary regions in CCTO ceramics. Our main objective has been to reduce the dielectric loss (together with the increase of the dielectric constant) in CCTO ceramics by decreasing the leakage current, due to the reduction in the grain boundaries conductivity. This has been done by reducing the CuO phase, with semiconducting behavior [23], and the formation of  $\text{CaTiO}_3$  and  $\text{Co}_2\text{TiO}_4$  phases with good dielectric insulating properties [24–26] in the grain boundaries, through substitution of  $\text{Co}^{2+}$  in  $\text{Cu}^{2+}$  site in CCTO ceramic. To find out the effect of substituting  $\text{Cu}^{2+}$  by  $\text{Co}^{2+}$  on the dielectric constant and loss values, we have investigated the microstructure of the grain boundaries in detail.

## 2. Experimental

### 2.1. Materials and method

$\text{Ca}(\text{NO}_3)_2 \cdot 4\text{H}_2\text{O}$  (purity 98%, Merck),  $\text{Cu}(\text{NO}_3)_2 \cdot 3\text{H}_2\text{O}$  (purity 99%, Merck),  $\text{Co}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  (purity 97%, Merck),  $\text{TiO}_2$  (purity 99.5%, Merck) and citric acid (purity 99.5%, Merck) were used as the starting materials and distilled water as the solvent. Proper amounts of these materials were selected based on the  $\text{CaCu}_{3-x}\text{Co}_x\text{Ti}_4\text{O}_{12}$  (CCCTO) ( $x = 0, 0.2, 0.4$  and  $0.6$ ) formula. First, a solution of the nitrates was prepared and, at the same time, the suspension of  $\text{TiO}_2$  powder and citric acid was made using minimum amounts of water. The amount of citric acid was chosen equivalent to the metal cations and the nitrates solution was added to the suspension. The final solution was kept at  $70\text{--}80^\circ\text{C}$  temperature, under vigorous stirring, and then dried in an oven at  $90^\circ\text{C}$  for 12 h, until a blue gel was obtained. The gel was calcined at  $850^\circ\text{C}$  for 8 h in a muffle furnace. After grinding the calcined powder, it was pressed into pellets with 10 mm in diameter and 2 mm in thickness, under 250 MPa using a hydraulic press. Finally, the prepared disks were sintered in air at  $1050^\circ\text{C}$  for 15 h.

### 2.2. Characterization methods

The X-ray diffractometer (XRD- D8 ADVANCED-BRUKER) with Cu  $K\alpha_1$  radiation ( $\lambda = 1.5406 \text{ \AA}$ ) was employed to investigate the crystal structure of the prepared samples. Scanning electron microscopy (SEM- LEO 1450VP) equipped with energy dispersive X-ray analyzer (EDX- OXFORD) was used to study the surface morphology and the local elemental analysis of the grains and grain boundaries. To measure the dielectric properties of the prepared

ceramics, both faces of the disks were coated with silver paste and cured in the hot air oven at  $220^\circ\text{C}$  for 2 h. The LCR meter (LCR 811 0G INSTEK) was used to measure the dielectric constant and the  $\tan\delta$  in the frequency range of 50 Hz–200 kHz at room temperature as well as at 1 kHz in the temperature range of  $300\text{--}600 \text{ K}$ .

## 3. Results and discussion

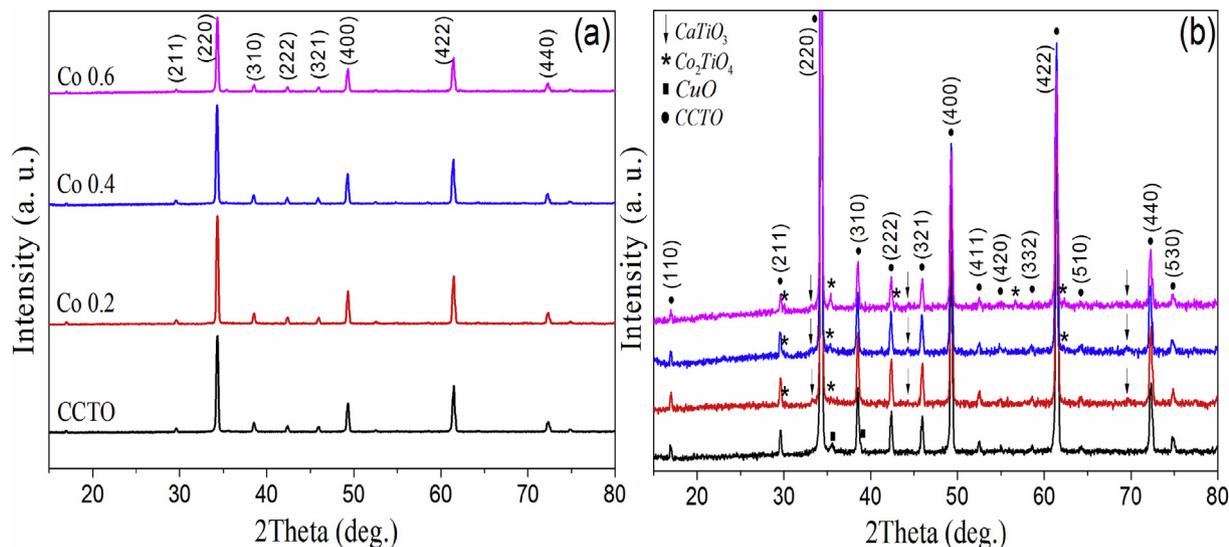
### 3.1. X-ray diffraction analysis

Fig. 1(a and b) illustrates the X-ray diffraction patterns of the  $\text{CaCu}_{3-x}\text{Co}_x\text{Ti}_4\text{O}_{12}$  (CCCTO) ceramics ( $x = 0, 0.2, 0.4$  and  $0.6$ ) sintered at  $1050^\circ\text{C}$  for 15 h. As the patterns show, the CCTO cubic crystal phases with the space group  $Im\bar{3}$  have been formed in accordance with JCPDS card No. 21-0140, in all prepared samples. It is obvious that the peaks of CuO phase can only be observed in the undoped sample. By adding cobalt into CCTO, the peaks related to  $\text{CaTiO}_3$  and  $\text{Co}_2\text{TiO}_4$  structures appear. The intensities of  $\text{CaTiO}_3$  and  $\text{Co}_2\text{TiO}_4$  peaks are enhanced by increasing the cobalt concentration.

### 3.2. Microstructural studies

The back scattered electron SEM images and their corresponding grain size histograms are presented in Fig. 2, which illustrates the surface morphology of the prepared ceramics. These figures indicate that with the increase in  $\text{Co}^{2+}$  concentration from  $x = 0$  up to  $x = 0.4$ , the size of the grains first becomes larger and thereafter decreases for  $x = 0.6$  as shown in Fig. 2(b, c and d). Furthermore, the exfoliated sheets with lighter color in the images are appeared between the grains mainly due to the presence of Cu-rich phase (CuO) [27,28]. Also this is proved by the EDX results. It is believed that the densification of the ceramics is somehow caused by the liquid phase that is formed during the sintering step [16,29]. By comparing the SEM images of the pure and cobalt doped samples, it can be concluded that the amount of the Cu-rich phase has been reduced remarkably in the doped samples along with the formation of  $\text{Co}_2\text{TiO}_4$  and  $\text{CaTiO}_3$  at the grain boundaries. These results are also confirmed by EDX, as shown in Fig. 3 (lower shapes are for the grains and upper ones for the grain boundaries, shown with yellow arrows) as well as the XRD analysis (Fig. 1(b)). The average grain size values of the samples with  $x = 0, 0.2, 0.4$  and  $0.6$  are found about 48, 108, 107 and  $75 \mu\text{m}$ , respectively. First, by increasing the cobalt concentration the CuO secondary phase (light color in Fig. 2(b and c)) decreases at the grain boundaries, which results in speeding up the grain growth. So, the grains become larger for the samples with  $x = 0.2$  and  $0.4$ . When the amount of cobalt concentration increases further and passes the critical limit ( $x = 0.6$ ), the amounts of  $\text{CaTiO}_3$  and  $\text{Co}_2\text{TiO}_4$  secondary phases, which have already appeared at the grain boundaries in the samples with  $x = 0.2$  and  $x = 0.4$  increase, causing the grain growth limitation. XRD results, Fig. 1(b), confirmed the decrease of the CuO as well as increasing the amounts of  $\text{CaTiO}_3$  and  $\text{Co}_2\text{TiO}_4$  phases. This phenomenon is called the pinning effect, which says that the critical grain size depends on the definite volume fraction of the secondary phases in the grain boundaries. So that, for the amounts of more than this definite volume fraction, further growth of the grains is inhibited and pinned [30–33]. This phenomenon seems to occur for the sample with  $x = 0.6$ .

The giant grains observed in our samples have also been reported by some other researchers [13,34,35]. As mentioned earlier, other researchers have reported that the presence of the Cu-rich phase at the grain boundaries is an important factor which affects the  $\tan\delta$  value. The grain boundaries were investigated further by using SEM and EDX. Fig. 3 is the back scattered electron SEM images of the grains and grain boundaries of the ceramic samples along



**Fig. 1.** X-ray diffraction patterns of (a)  $\text{CaCu}_{3-x}\text{Co}_x\text{Ti}_4\text{O}_{12}$  ceramics sintered at  $1050^\circ\text{C}$  for 15 h and (b) the corresponding expanded patterns. The peaks are indexed for cubic structure of CCTO.

with their EDX. As it can be seen in Fig. 3(a), for the pure sample the thickness of the grain boundaries and the amount of the Cu-rich phase are remarkably large, compared to the doped samples (Fig. 3(b–d)). These figures show that by increasing the amount of  $\text{Co}^{2+}$ , from  $x = 0.2$  to  $x = 0.6$ , the thickness of the grain boundaries and also the amount of the Cu-rich phase have been reduced, and at the same time,  $\text{Co}_2\text{TiO}_4$  and  $\text{CaTiO}_3$  phases have been formed at the grain boundaries. These results are further confirmed by the XRD analysis (Fig. 1(b)). The EDX of the grains (Fig. 3, lower shapes) indicates that by increasing the amount of  $\text{Co}^{2+}$  dopant, only the amount of  $\text{Co}^{2+}$  in the grains has increased, while at the grain boundaries (Fig. 3, upper shapes) the Cu-rich phase decreased along with the formation of  $\text{Co}_2\text{TiO}_4$  and  $\text{CaTiO}_3$  phases.

### 3.3. Bulk density determination

The bulk densities of the prepared ceramics were determined 4.85, 4.65, 4.61 and  $4.52\text{ g/cm}^3$  for the samples with  $x = 0, 0.2, 0.4$  and  $0.6$ , respectively using Archimedes method. The density of the ceramic pellets slightly decreased with the increase of  $\text{Co}^{2+}$  concentration, since the atomic weight of cobalt (58.93 g) is smaller than that of copper (63.54 g). Moreover, as mentioned earlier, in the sintering process the second liquid phase at the grain boundaries results in the densification of the pellets. However, since the thickness of the secondary phase has remarkably decreased in doped samples, the density of the pellets was reduced by increasing the cobalt dopant concentration, in agreement with some other reports [16,29], which is confirmed by the SEM images (Fig. 2).

### 3.4. Dielectric property studies

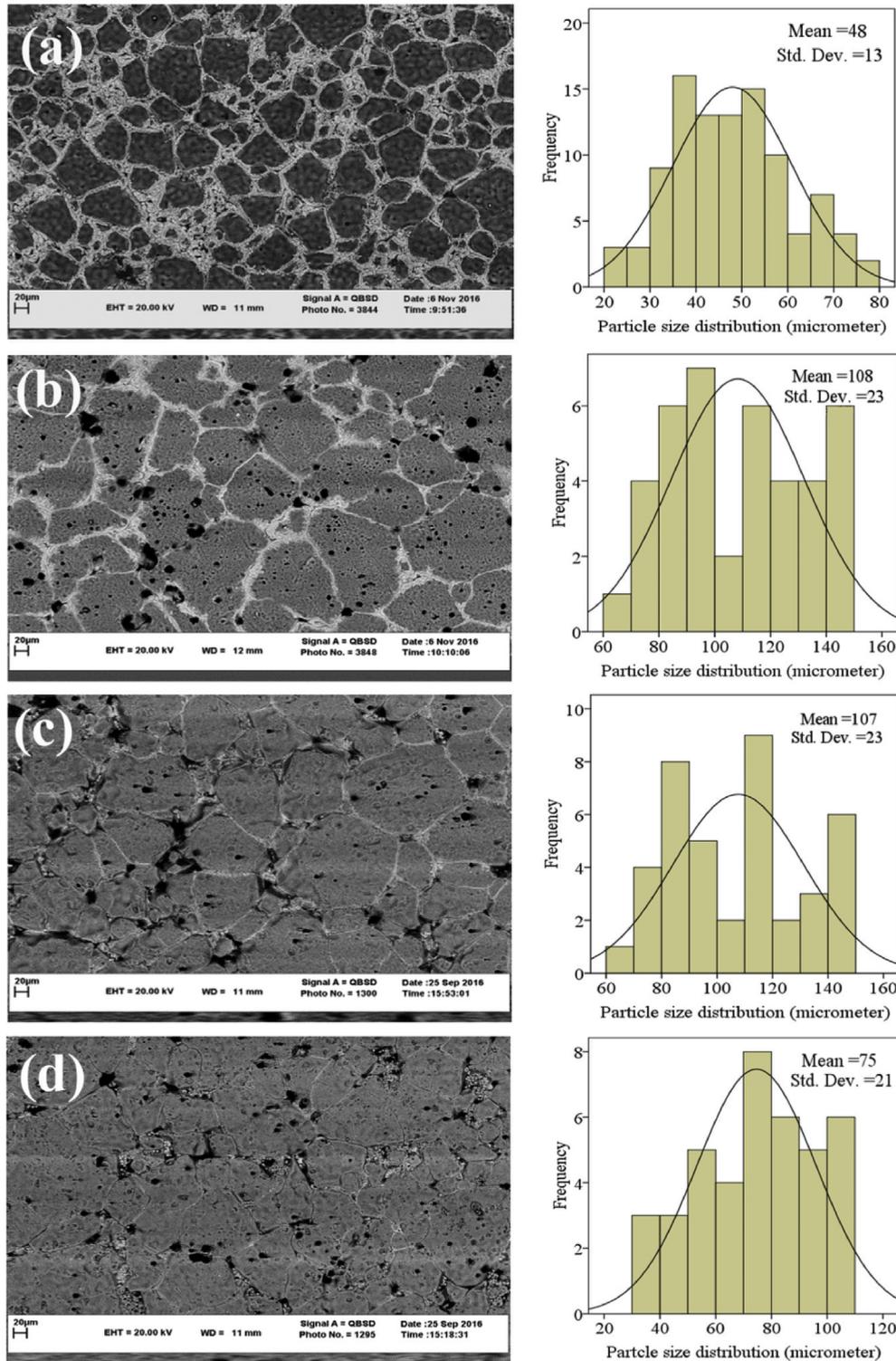
The effect of temperature on the dielectric constant and  $\tan\delta$  of the prepared samples was investigated at 1 kHz in the temperature range of 300–600 K, Fig. 4(a and b). The dielectric constants obtained for all the samples were greater than  $10^4$ , in the whole range of temperature. As it can be seen in Fig. 4(a), from room temperature to about 400 K no remarkable changes can be observed in the dielectric constant of the samples. However, at temperatures close to room temperature, the dielectric constants of the doped samples are greater than that of the undoped sample, while the dielectric losses are less. This is observed more clearly in the insets of Fig. 4(a

and b). At temperatures above 450 K, the dielectric constant of the samples enhances with the increase of the temperature, which is highly noticeable for the samples with  $x = 0.4$  and  $x = 0.6$ . The big differences in the dielectric values at high and low temperatures can be related to the movement difference of the dipoles at high and low temperatures. These remarkable increase in the dielectric constant at high temperatures along with the increase of loss is due to the high-temperature dielectric relaxation of CCTO ceramics, as has been reported previously [36,37].

In fact in an undoped sample,  $\text{CaTiO}_3$  and  $\text{Co}_2\text{TiO}_4$  compounds with high polarization properties [24–26] do not exist, but as shown in Fig. 1 (b)  $\text{CuO}$  phase with semiconducting behavior [23] is detected. So, by increasing the temperature above 450 K, the conductivity in the grain boundaries increases which is probably due to the presence of  $\text{CuO}$ , with semiconducting behavior, at the grain boundaries. This leads to a reduction in the grain boundary resistance ( $R_{gb}$ ), causing a decrease in the difference between the semiconducting grain resistance ( $R_g$ ) and the grain boundary resistance ( $R_{gb}$ ). This results in less polarization at the grain boundaries, leading to the low dielectric constant. This process is a limiting factor for increasing the dielectric constant in the undoped sample compared to the doped samples at high temperatures, Fig. 4(a). Since with bigger  $R_{gb}$  more difference between  $R_{gb}$  and  $R_g$  appears, which results in stronger interfacial polarization leading to the increase in the dielectric constant [16]. Our results showed that in an undoped sample with high  $\text{CuO}$  content, the dielectric constant is lower in comparison with the samples with very low or without amount of  $\text{CuO}$  (doped samples) which is in agreement with the other report [22].

On the other hand, in our cobalt doped samples by increasing the cobalt concentration, the polar phases of  $\text{CaTiO}_3$  and  $\text{Co}_2\text{TiO}_4$  have increased as shown in Fig. 1(b). Therefore it can be said that due to the polarity and also the relaxation behavior in the present titanate compounds [26,38], the dielectric constant in the doped samples enhances by increasing the temperature (which is more remarkable for the samples with  $x = 0.4$  and  $0.6$  having larger amounts of  $\text{CaTiO}_3$  and  $\text{Co}_2\text{TiO}_4$  phases), compared to the undoped sample which can be seen in Fig. 4(a).

Regarding what mentioned above; the existence of these phases decreases the conductivity at the grain boundaries in the doped ceramics ( $\text{CuO}$  amount decreases and at the same time,  $\text{CaTiO}_3$  and

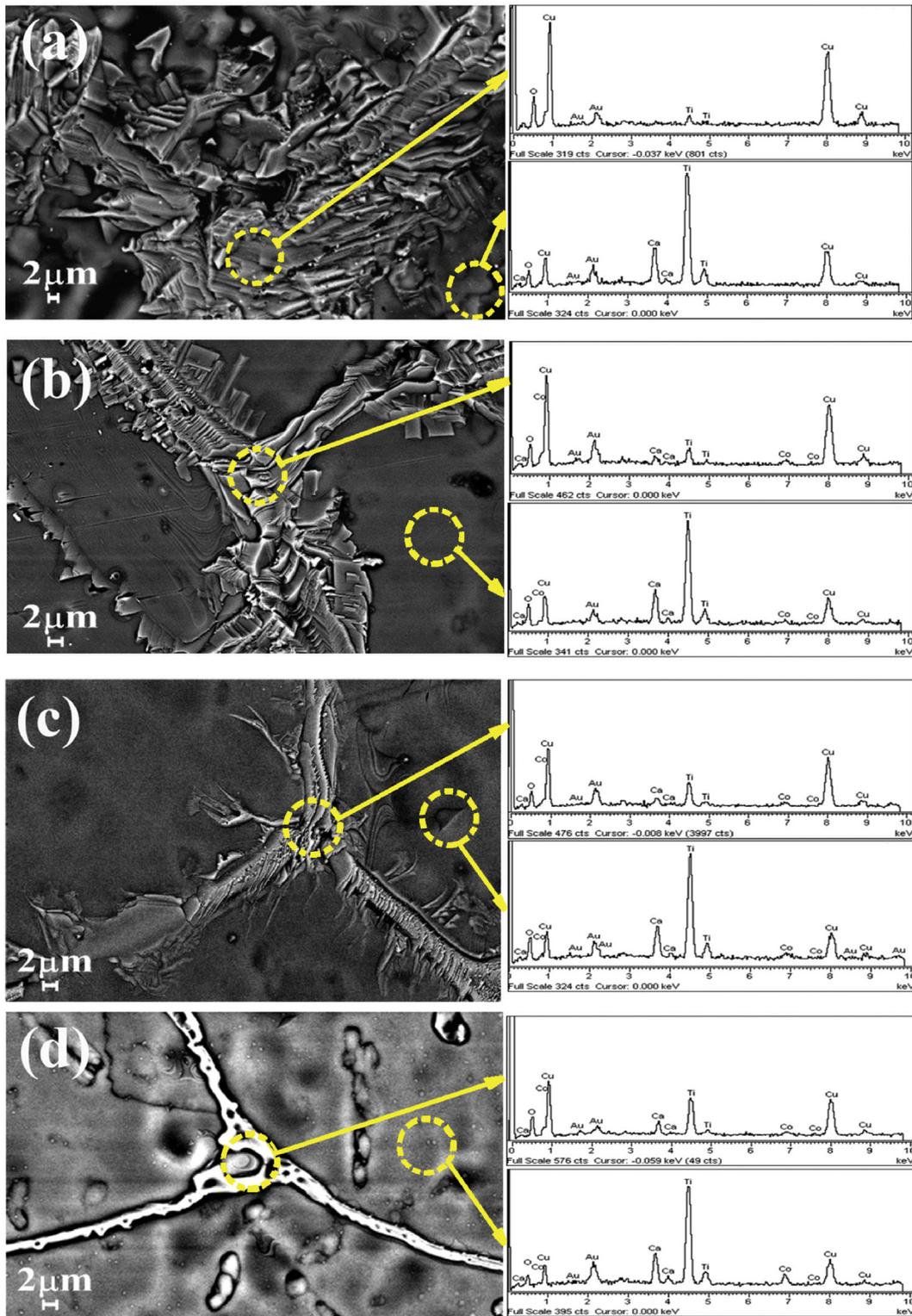


**Fig. 2.** Back scattered electron SEM images of  $\text{CaCu}_{3-x}\text{Co}_x\text{Ti}_4\text{O}_{12}$  samples (a)  $x = 0$ , (b)  $x = 0.2$ , (c)  $x = 0.4$  and (d)  $x = 0.6$ , sintered at  $1050^\circ\text{C}$  for 15 h, and the corresponding histograms.

$\text{Co}_2\text{TiO}_4$  phases with good dielectric insulating behavior increase). So, the dielectric loss which is directly related to the grain boundary conductivity [10–12], becomes lower in the doped samples compared to the undoped sample by increasing the temperature, as shown in Fig. 4(b).

Fig. 5(a and b) shows the dielectric constant and  $\tan\delta$  for the

$\text{CaCu}_{3-x}\text{Co}_x\text{Ti}_4\text{O}_{12}$  ( $x = 0, 0.2, 0.4$  and  $0.6$ ) ceramics as a function of frequency, respectively. As Fig. 5(a) shows, the dielectric constant of the undoped sample at room temperature, is almost constant throughout the frequency range, which reveals that the CCTO dielectric constant is frequency independent, in agreement with previous research [39]. However, by doping  $\text{Co}^{+2}$  into the CCTO



**Fig. 3.** Back scattered electron SEM images of  $\text{CaCu}_{3-x}\text{Co}_x\text{Ti}_4\text{O}_{12}$  samples (a)  $x = 0$ , (b)  $x = 0.2$ , (c)  $x = 0.4$ , (d)  $x = 0.6$ , and their EDX analysis localized on the grains and grain boundaries (lower shapes are for the grains and upper ones for the grain boundaries, shown with yellow arrows). (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

ceramic, the frequency dependence of the dielectric constant becomes remarkable, which is more significant for the frequencies less than 1 kHz. Similar results have been obtained for CCTO, in which  $\text{Cu}^{2+}$  was substituted by  $\text{Fe}^{3+}$  [40]. The values of the

dielectric constant in our samples were found higher than  $10^4$ , in all frequency range of 50 Hz–200 kHz. At 50 Hz, the dielectric constant values of the doped samples with  $x = 0.2, 0.4$  and  $0.6$ , were about  $5.4 \times 10^4, 5.9 \times 10^4$  and  $4.5 \times 10^4$ , respectively, which are

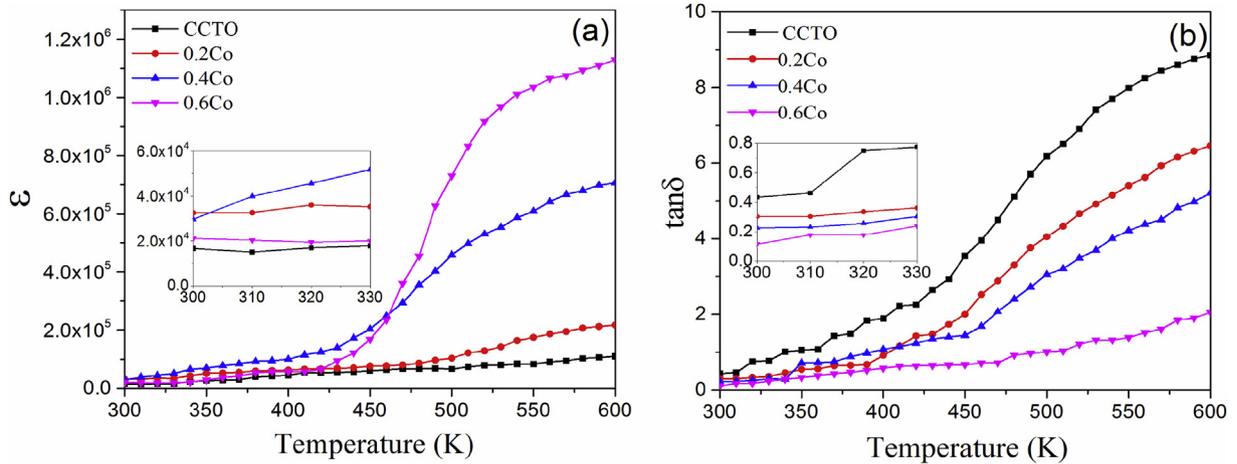


Fig. 4. Temperature dependence of (a) dielectric constant and (b) dielectric loss in  $\text{CaCu}_{3-x}\text{Co}_x\text{Ti}_4\text{O}_{12}$  ceramics, at 1 kHz.

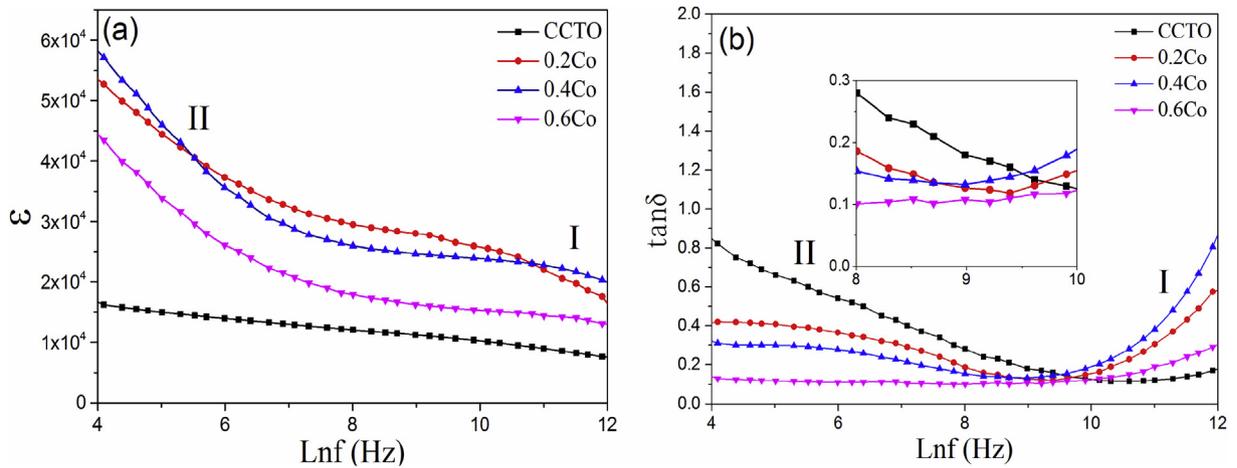


Fig. 5. Frequency dependence of (a) dielectric constant and (b) dielectric loss in  $\text{CaCu}_{3-x}\text{Co}_x\text{Ti}_4\text{O}_{12}$  samples, at room temperature.

remarkably larger than that of the undoped sample ( $1.7 \times 10^4$ ). As Fig. 5(a and b) illustrates, there are two dielectric relaxation processes at high and low frequencies (I and II) in both of the dielectric constant and  $\tan\delta$ . Relaxation I, which is observed at about 100 kHz, is related to Debye-type relaxation [41]. The second relaxation starts at about 100 Hz. It has been reported that the increase in the dielectric constant by decreasing the frequency results from interfacial and Maxwell-Wagner polarization, which occurs in the CCTO ceramics and is a very important factor for the enhancement of the dielectric constant at low frequencies [39]. Fig. 5(b) shows that for frequencies below 20 kHz, the  $\tan\delta$  decreases by increasing the  $\text{Co}^{2+}$  dopant concentration. This  $\tan\delta$  reduction is very large for the sample with  $x = 0.6$ , ( $\tan\delta = 0.15$ ), comparing to the value for the undoped sample ( $\tan\delta = 0.87$ ) at 50 Hz. For more clarity, the frequency dependence of  $\tan\delta$  is given in the inset of Fig. 5(b), in the range of 3–20 kHz. For frequencies greater than 20 kHz, the  $\tan\delta$  is frequency dependent, as shown in Fig. 5(b). The fast increase in  $\tan\delta$  at higher frequencies is due to the Debye relaxation [13]. The behavior of the dielectric constant and  $\tan\delta$  in the CCTO ceramic has been explained by IBLC model, in which the dielectric constant ( $\epsilon$ ) is given by the following equation [42–44]:

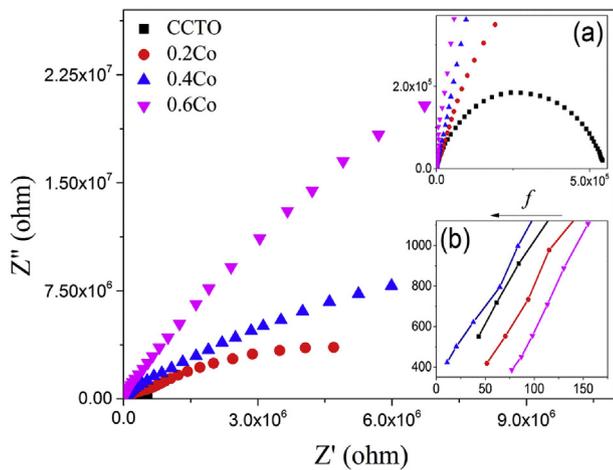
$$\epsilon_r = \epsilon_{gb} \left( d_g + d_{gb} / d_{gb} \right) \quad (1)$$

where  $\epsilon_{gb}$  is the grain boundary dielectric constant,  $d_g$  is the grain

size and  $d_{gb}$  is the thickness of the grain boundary. As this equation indicates, the size of the grains plays an important role in the value of the dielectric constant. It is worth mentioning that it is not possible to obtain the exact value of the dielectric constant in the grain boundary ( $\epsilon_{gb}$ ) regions, since it is impossible to calculate the thickness and the cross-sectional area of these regions accurately [45]. According to the SEM images (Fig. 2), with the increase in  $\text{Co}^{2+}$  dopant concentration up to  $x = 0.4$ , the average size of the grains becomes larger (Fig. 2(b and c)). However, by increasing  $\text{Co}^{2+}$  concentration to  $x = 0.6$  the average size of the grains becomes smaller (Fig. 2(d)), but is still larger than that of the undoped sample. Therefore, considering Eq. (1), one can conclude that the samples with larger grains and thinner grain boundaries, which is confirmed by the experimental results, have the higher dielectric constants [42,46].

Fig. 6 shows the Cole-Cole plots of the impedance, which can explain the  $\tan\delta$  behavior of the prepared  $\text{CaCu}_{3-x}\text{Co}_x\text{Ti}_4\text{O}_{12}$  at room temperature. The overlapped region of these curves are amplified and presented as the inset Fig. 6(a), for more clarity. By fitting the arc data, the resistance of the grains ( $R_g$ ) and the grain boundaries ( $R_{gb}$ ) are obtained at high and low frequencies, respectively (given in Table 1). The experimental frequency increases along the direction of the arrow in Fig. 6(b).

According to IBLC model, the  $\tan\delta$  at low frequencies, given by the following equation [15,43]:



**Fig. 6.** The Cole-Cole plot of impedance for  $\text{CaCu}_{3-x}\text{Co}_x\text{Ti}_4\text{O}_{12}$  samples, at room temperature. The inset (a) illustrates the amplification of the overlapped region of these curves, and the inset (b) illustrates an enlarged view of the data close to the origin for the highest frequency.

$$\tan\delta \approx 1/\omega R_{gb}C_p(\epsilon) \quad (2)$$

where  $R_{gb}$  denotes the grain boundary resistance and can be determined at low frequencies by the extrapolated intercept of the arc on the  $Z'$  axis [47,48], while  $C_p(\epsilon)$  is the sample capacitance, which is proportional to the dielectric constant value ( $\epsilon$ ), related to Eq. (1). As seen in Fig. 6, at low frequencies,  $R_{gb}$  in Eq. (2) enhances with the increase in  $\text{Co}^{2+}$  concentration. The values of  $R_{gb}$  obtained for an undoped and the doped ( $x = 0.2, 0.4$  and  $0.6$ ) samples are  $5.5 \times 10^5 \Omega$ ,  $9.5 \times 10^6 \Omega$ ,  $3 \times 10^7 \Omega$  and  $3.2 \times 10^8 \Omega$ , respectively (given in Table 1). The increase in the resistance by increasing  $\text{Co}^{2+}$  is mainly due to the decrease of the Cu-rich phase (CuO) and the formation of  $\text{CaTiO}_3$  and  $\text{Co}_2\text{TiO}_4$  phases at the grain boundaries, as mentioned earlier. According to Eq. (2), both  $R_{gb}$  and  $C_p(\epsilon)$  affect the value of the  $\tan\delta$  at low frequencies. Our results show that the undoped sample has the least value of  $R_{gb}$  and  $C_p(\epsilon)$  and thus, the  $\tan\delta$  is the highest compared to the doped samples, as can be seen in Fig. 5(b). However, the sample with  $x = 0.6$  has the highest  $R_{gb}$  among all the samples, so it is expected that its  $\tan\delta$  decreases. Since,  $C_p(\epsilon)$  for this sample ( $x = 0.6$ ) is smaller than that of the other two doped samples, according to Eq. (2), the  $\tan\delta$  is expected to increase. Nevertheless, since the  $\tan\delta$  for the sample with  $x = 0.6$  is the smallest among all the other samples, we can conclude that in Eq. (2),  $R_{gb}$  is the dominant factor in reducing the dielectric loss in the doped samples at low frequencies, which is in agreement with other study [49]. Actually, at low frequencies, dc conductivity at the grain boundaries which is associated with  $R_{gb}$ , results in  $\tan\delta$  [50]. Our impedance spectroscopy analysis results confirm this explanation.

At high frequencies, the  $\tan\delta$  is approximately given as [15,43]:

$$\tan\delta \approx \omega R_g C_p(\epsilon) \quad (3)$$

**Table 1**  
The resistance of grains and grain boundaries of  $\text{CaCu}_{(3-x)}\text{Co}_x\text{Ti}_4\text{O}_{12}$  Ceramics [ $x = 0, 0.2, 0.4$  and  $0.6$ ].

Sample	$R_g(\Omega)$	$R_{gb}(\Omega)$
$\text{CaCu}_3\text{Co}_0\text{Ti}_4\text{O}_{12}$	43	$5.5 \times 10^5$
$\text{CaCu}_{2.8}\text{Co}_{0.2}\text{Ti}_4\text{O}_{12}$	52	$9.5 \times 10^6$
$\text{CaCu}_{2.6}\text{Co}_{0.4}\text{Ti}_4\text{O}_{12}$	11	$3 \times 10^7$
$\text{CaCu}_{2.4}\text{Co}_{0.6}\text{Ti}_4\text{O}_{12}$	77	$3.2 \times 10^8$

where  $R_g$  denotes the semiconducting grain resistance, and can be estimated by nonzero intercept of the  $Z'$  axis which is shown in the inset of Fig. 6(b). The grain resistance of the all samples is found to be small in the range of 11–77  $\Omega$ , given in Table 1, which is agreement with others results [51,52]. As it can be seen in Fig. 5(a), changes in  $C_p(\epsilon)$  is remarkable compared to  $R_g$  at high frequencies. Therefore, in Eq. (3),  $C_p(\epsilon)$  is the dominant factor in increasing the  $\tan\delta$  in the doped samples, at high frequencies. As Fig. 5(a) shows the dielectric constant values of the doped samples are higher than that of the undoped sample, similar arguments can explain why the  $\tan\delta$  value is smaller for the undoped sample at high frequencies (Fig. 5(b)). So, it can be said that at high frequencies there is a reasonable correlation between the  $\tan\delta$  and the capacitance ( $C_p(\epsilon)$ ). It is also evident from Fig. 5(b) that at frequencies higher than 20 kHz, the  $\tan\delta$  increases with the increasing frequency for all samples, according to Eq. (3). However, it is obvious that at low frequencies (<1 kHz) the decrease of the  $\tan\delta$  is very significant. The values of the  $\tan\delta$  in the sample with  $x = 0.6$  and the undoped sample at 50 Hz frequency are about 0.15 and 0.87, respectively. So, the dielectric loss has decreased about 8 times, at low frequencies. As mentioned before, the lower  $\tan\delta$  for the doped samples at low frequencies is due to the reduction in the Cu-rich phase (CuO) and the formation of  $\text{CaTiO}_3$  and  $\text{Co}_2\text{TiO}_4$  phases at the grain boundaries (as shown in XRD patterns, SEM images and grain boundary EDX results), leading to the higher resistance at the boundaries. Since in our samples, the values of  $R_g$  are much less than  $R_{gb}$  as given in Table 1. Thus, according to IBL model, this big difference between  $R_g$  and  $R_{gb}$  leads to a large polarization at the grain boundaries, causing the giant dielectric constant in CCTO [40]. The greater the difference is between  $R_{gb}$  and  $R_g$ , the stronger the interfacial polarization will be, leading to the increase in the dielectric constant [16]. Our results indicate that doping  $\text{Co}^{2+}$  into the CCTO ceramics enhances the resistance of the grain boundaries, and therefore, the dielectric constant of the doped samples becomes higher than that of the undoped sample.

The effect of the cobalt dopant concentration on the dielectric constant and  $\tan\delta$  at different frequencies for all the samples are given in Fig. 7(a and b), respectively. As can be seen in Fig. 7(a), the samples with  $x = 0.2$  and  $x = 0.4$  have larger dielectric constant values. Furthermore, the dielectric constant seems to become independent from cobalt dopant concentration, with the increase in the frequency. As Fig. 7(b) shows, the  $\tan\delta$  of the undoped sample is larger than that of the doped samples, at low and middle frequencies (50 Hz–1 kHz). However, at 10 kHz, the  $\tan\delta$  is almost independent of the cobalt concentration. The  $\tan\delta$  of the sample with  $x = 0.4$  has a maximum value at higher frequencies. So, we can conclude that the concentration of cobalt dopant is an important factor considering the dielectric properties of the CCTO ceramics.

#### 4. Conclusion

In this study, ceramics of  $\text{CaCu}_{3-x}\text{Co}_x\text{Ti}_4\text{O}_{12}$  (CCCTO,  $x = 0, 0.2, 0.4$  and  $0.6$ ) were fabricated by a semi-wet route and the effects of substituting  $\text{Cu}^{2+}$  by  $\text{Co}^{2+}$  on the dielectric properties of the prepared samples were investigated. The samples were characterized using XRD, SEM and EDX techniques. The dielectric properties of the prepared samples were studied using a LCR meter, at different temperatures and frequencies. Our results showed that the dielectric constant of the samples increased with the increase in cobalt dopant concentration, while the dielectric loss decreased. These observations can be related to the reduction in the Cu-rich (CuO) phase and also the formation of  $\text{CaTiO}_3$  and  $\text{Co}_2\text{TiO}_4$  phases at the grain boundaries, which lead to the decrease in the grain boundaries conductivity. These results were confirmed by the XRD, SEM, EDX and also impedance spectroscopy (IS). Therefore, it can

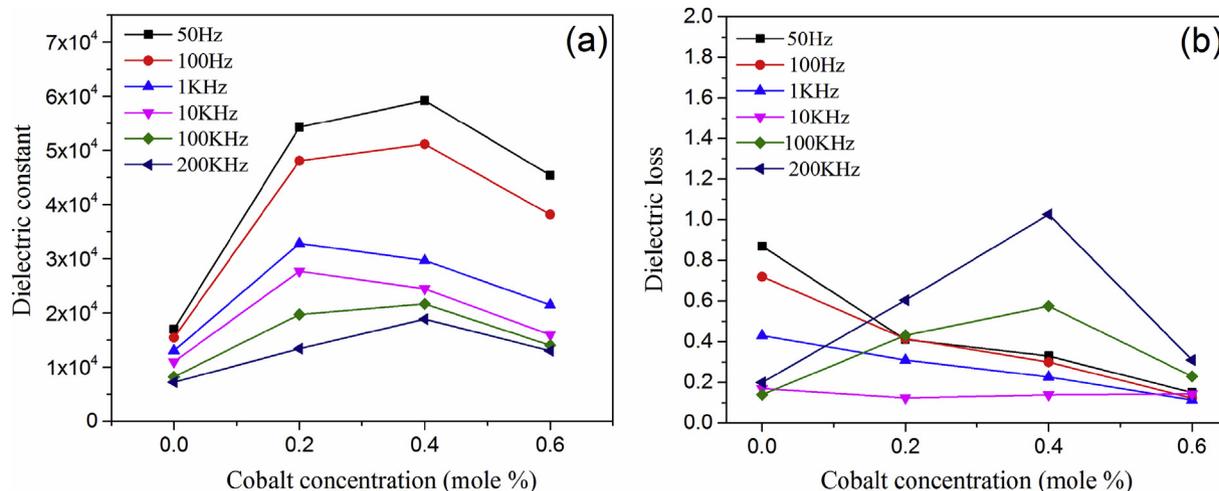


Fig. 7. The effect of cobalt dopant concentration on the (a) dielectric constant and (b) dielectric loss, at different frequencies.

be said that the substitution of  $\text{Cu}^{2+}$  by  $\text{Co}^{2+}$  in the CCTO ceramics enhances the dielectric constant in a broad range of frequencies and temperatures as well as decreasing the dielectric loss ( $\tan\delta$ ) at low and middle frequencies, significantly. Regarding the application of CCCTO ceramics, we can conclude that for application in devices working in the temperature range of 300–600 K, the doped sample with  $x = 0.6$  cobalt concentration seems to be the best composition. This sample shows the highest increase in the dielectric constant and also the highest decrease in the dielectric loss with increasing the temperature among the all prepared samples. Furthermore, for the devices working in a frequency range up to 20 kHz, particularly at urban power frequency, the sample with  $x = 0.4$  cobalt concentration can be suggested to be the best composition, Because it shows the highest dielectric constant and also the lowest dielectric loss, in comparison with the other samples.

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