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## Precise Evaluation the Effect of Microwave Irradiation on the Properties of Palm Kernel Oil Biodiesel Used in a Diesel Engine

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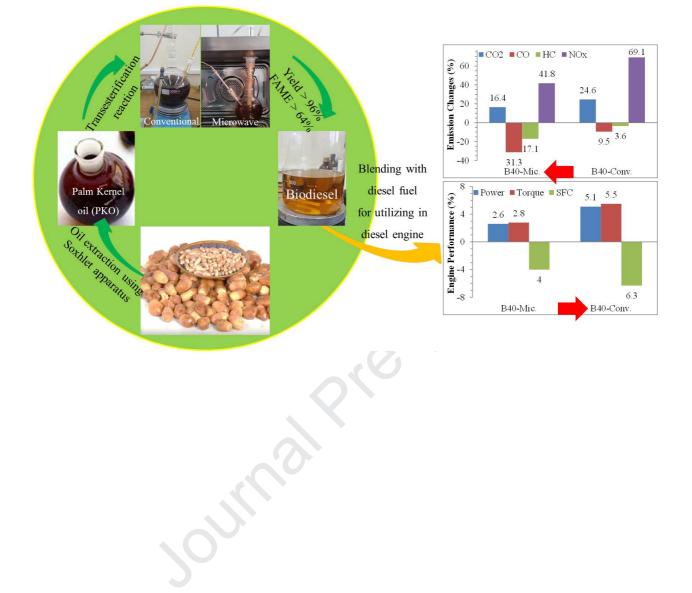
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5

### 6 Abstract

7 Palm kernel oil (PKO) has an appropriate oil content which can be utilized for biodiesel production. Sparse studies have been performed on its ability as well as the produced 8 9 biodiesel properties and performance in the diesel engine. Further, no study has been 10 performed on the conversion of PKO via microwave irradiation and comparing the PKO biodiesel abilities combusted in diesel engines with those prepared by conventional methods. 11 12 For this purpose, PKO was directly extracted from date palm fruits (Phoenix dactylifera) with 13 microwave and conventional heating systems utilized for conversion of PKO to biodiesel. In addition to optimization of microwave-assisted transesterification reaction conditions, 14 15 variations of temperature during each run were carefully monitored. The results revealed that palm kernel has 10 wt.% of oil containing high unsaturated fatty acids and free fatty acid 16 17 (FFA). The transesterification reaction was sharply accelerated by microwave power such 18 that the reaction time diminished from 90 min for conventional method to 2.5 min. The 19 results of temperature monitoring confirmed great elevation in the reaction temperature (over 20 boiling point of methanol) with the rise of microwave power and methanol/oil ratio. 21 Moreover, reduction of temperature occurred with more loading of catalyst due to greater formation of soap. Both high and low temperatures showed negative effects on the yield of 22 23 transesterification reaction. The performance and emissions gas evaluation of the engine fueled by PKO biodiesel produced by microwave and conventional heating system indicated 24



that the fuel produced by microwave irradiation can sharply reduce the CO and HC and insignificantly increase  $NO_x$  in exhaust emission as compared to fuel produced by the conventional method. Also, higher amounts of microwave-assisted produced PKO biodiesel can be blended with net diesel fuel to use in diesel engines. The results suggested that microwave irradiation can considerably influence the phytochemical properties of biodiesel and improve its combustion profile in the diesel engine and exhaust gas emissions.

31

32 Keywords: Palm kernel oil (PKO); Microwave irradiation; Biodiesel; Engine performance,
33 Exhaust emissions.

34

#### 35 **1. Introduction**

The world production of dates has increased considerably over the last 30 years. 36 Nowadays, palm fruits are widely cultivated around the world especially in Middle East 37 which produces around 91% of the world's dates (Ali et al. 2015). Increasing in the palm 38 39 production has caused the palm oil to claim the first rank in the amount of oil produced in the 40 world (Rupilius and Ahmad 2007). Palm kernel, as an important by-product from the process 41 of palm oil production, can be a suitable source for biodiesel production given its appropriate 42 oil content (Jamil et al. 2017). The researchers have reported that the palm kernel has 5-12% oil depending on its type and cultivating conditions. Palm kernel oil (PKO) presents different 43 44 compositions with most of them possessing high unsaturated carbon bonds, although the 45 saturated short-chain fatty acids have also been detected (Lin et al. 2008, Bello et al. 2015).

Biodiesel contains fatty acid alkyl (methyl) ester (FAME) which is usually produced by transesterification of triglycerides with methanol in the presence of a catalyst. This fuel is non-toxic, biodegradable, sulfur and aromatics free compound which is of high interest due to



49 environmental problems caused by consumption of petroleum fuels such as air pollution,

50 global warming, and climate change (Chuah et al. 2017, Mahmudul et al. 2017).

51 The researchers have been trying to find new sources as feedstock for biodiesel production 52 to reduce the biodiesel production cost (Phoon et al. 2017, Ong et al. 2019, Xie et al. 2019). In this case, palm oil has been extensively evaluated in the transesterification reaction and 53 54 tested in the diesel engine (Abdul Kapor et al. 2017, Fazal et al. 2018, Bautista et al. 2019). However, fewer studies have been performed on the biodiesel production from PKO and its 55 ability in the diesel engine. Aladetuyi et al. (2014) studied the reaction conditions of biodiesel 56 production from PKO and obtained 90% yield at the conditions of 100 °C, 2 h reaction time, 57 58 1 wt.% of catalyst (KOH) and oil-methanol ratio of 5:1 (w/v). Bello et al. (2015) reported that 59 PKO biodiesel produced at the conditions of 60 °C, catalyst-to-oil ratio of 0.24:1 (w/v), and oil-methanol molar ratio of 10:1 contained 78% saturated fatty acid groups. Ojolo et al. 60 61 (2012) presented PKO transesterified at 55 °C, 5:1 (w/w) ratio of methanol-to-oil, 0.5 wt.% of catalyst (NaOH) and obtained a yield of 92%. In addition, PKO biodiesel production using 62 63 heterogeneous catalysts such as Al<sub>2</sub>O<sub>3</sub>-supporetd alkali earth metal oxides 64 (Benjapornkulaphong et al. 2009), Ca and Zn mixed oxide (Ngamcharussrivichai et al. 2008), sulfated zirconia and stannic oxide (Jitputti et al. 2006), and modified dolomites 65 66 (Ngamcharussrivichai et al. 2007) was also evaluated. However, higher reaction temperatures (over 100 °C), time (around 3 h), alcohol/oil molar ratio (around 15), and catalyst amount ( $\approx$ 67 68 10 wt.%) are required to achieve proper conversion of PKO to biodiesel, heterogeneously.

New technologies such as supercritical fluid (García-Martínez et al. 2017), microwave irradiation (Nayebzadeh et al. 2017) and ultrasonic wave (Hoseini et al. 2017) are utilized for biodiesel production, with microwave irradiation offering more desirable properties. Microwave energy makes a uniform heating profile at a molecular level in the materials whose thermal effects include a combination of heating rate, hot spots, and selective



74 absorption of radiation by polar substances (Hashemzehi et al. 2016). Due to the accelerated 75 reaction rate, milder reaction conditions, higher chemical yield, lower energy usage, and different reaction selectivity, microwave irradiation is widely used in today's industries 76 77 (Quirino et al. 2016). PKO biodiesel was tested in a diesel engine and offered a lower power, torque, and specific fuel consumption compared to diesel fuel (Lin et al. 2008, Bello et al. 78 79 2015). It can be related to high kinetic viscosity and low heating value of PKO which has a negative effect on the engine performance. On the other hand, B20 (20 vol.% biodiesel-80 80 vol.% net diesel) improved its properties (Igbokwe et al. 2015, Igbokwe and Nwafor 2016, 81 82 Shote et al. 2019).

However, to the best of our knowledge no study has been done on the conversion of PKO to biodiesel under microwave irradiation assessing the reaction conditions and variations of temperature during the reaction. In addition, the effect of microwave irradiation on the properties and performance of produced biodiesel in the diesel engine has not been evaluated either.

88 Therefore, in this study, microwave-assisted biodiesel production from PKO using NaOH 89 as homogeneous catalyst was assessed in detail. For this purpose, after extraction of PKO by 90 solvent extraction method via soxhlet apparatus, it was transesterified using microwave 91 irradiation and conventional method. The reaction conditions under microwave heating such 92 as microwave power, reaction time, methanol-to-oil molar ratio, and catalyst concentration 93 were optimized. In addition, the changes in the reaction temperature during each run were 94 monitored. Finally, the physicochemical properties of the PKO biodiesel produced via the two heating systems (microwave and conventional) along with their performance and exhaust 95 gas emissions in the diesel engine were evaluated. 96

97

#### 98 2. Materials and methods



99 The operation processes for production of biodiesel via two heating systems and testing100 them in the diesel engine is completely summarized in figure S1.

- 101
- 102 **2.1. Palm kernel oil extraction**

103 Date palm fruits (Phoenix dactylifera) were purchased from a local store. Then, their 104 kernel was separated from the pulp and washed completely with hot distillated water to eliminate the remaining pulp. After drying the kernels in the oven for overnight, they were 105 106 crushed to the particle with a diameter lower than 1 mm. Then, the solvent method via the Soxhlet apparatus was utilized for oil extraction where hexane was used as solvent with a 4 107 108 mL/1 g kernel ratio (Ali et al. 2015). After 8 h, the solvent was separated from the oil through 109 evaporation of mixture at 45 °C and 450 mm Hg. Finally, the yield and composition of PKO were obtained respectively in terms of the proportion of PKO weight to kernels' weight and 110 gas chromatography (GC) as well as other physical properties of PKO such as density 111 (ASTM D1298), viscosity (ASTM D445), acid value, and molecular weight. 112

- 113
- 114 **2.2. Biodiesel production process**

115 2.2.1. Esterification reaction

116 The extracted PKO includes high FFA contents which must be firstly esterified to reduce the FFA content due to sensitivity of alkali homogeneous catalyst to the amount of FFA 117 causing soap formation (Hashemzehi et al. 2016). Therefore, a two-stage process involving 118 119 esterification by acid catalyst and the transesterification by alkali catalyst is used for biodiesel 120 production from PKO (Zullaikah et al. 2005). The esterification reaction was performed under the conditions of 60 °C, 6 methanol/PKO molar ratio, 1 wt.% of catalyst (H<sub>2</sub>SO<sub>4</sub>), and 121 122 60 min reaction time (Aranda et al. 2008, Hayyan et al. 2010). After the reaction, the product 123 mixture was poured in the separation funnel to separate the oil and ester layer (bottom layer)

124 from the by-product layer (water and catalyst) using gravity (see Figure S2). Finally, the acid 125 value was measured to obtain the FFA content of esterified PKO, which met the standard 126 range.

127

128 2.2.2. Transesterification reaction

129 After reduction of the FFA content, the transesterification reaction was performed by two heating systems (conventional and microwave), as shown in Figure S3. The conventional 130 131 biodiesel production from PKO was carried out in a two-neck glass reactor coupled with a 132 condenser to condense the methanol from vapor to liquid phase and a thermocouple to sense 133 the reaction temperature. The reactor was poured with 1000 g PKO, 280 cc methanol (6 134 molar ratio of methanol/PKO) and 10 g NaOH as catalyst (1 wt.%). The reaction was performed at 60 °C for 90 min (Alamu et al. 2007, Lubes and Zakaria 2009). Since no study 135 136 had been carried out on the microwave-assisted biodiesel production from PKO, the reaction conditions were evaluated and optimized. The microwave-assisted transesterification reaction 137 138 was performed in a 100 mL two-neck glass reactor poured with 20 g of PKO and desirable 139 amounts of methanol and catalyst. Then, the reactor was placed in a modified domestic microwave oven (Daewoo, Model No. KOC9N2TB, 900 watts, 2.45 GHz) with a hole of 20 140 mm at its top to connect the glass reactor to a condenser for refluxing the methanol. The 141 142 transesterification reaction conditions of microwave power (90 180, 270 and 360 W), reaction time (1, 1.5, 2, 2.5 and 3 min), methanol/PKO molar ratio (3, 6, 9 and 12), and catalyst 143 144 concentration (0.5, 0.75, 1, 1.25 and 1.5 wt.%) were evaluated further.

After each reaction, the product mixture was poured in a decanter to separate the biodiesel (top layer) from glycerol as a by-product (see Figure S2). After elimination of methanol from the biodiesel layer through evaporation, the yield of reaction and FAME content of produced PKO biodiesel were measured by the following Eqs.:

	Journal Pre-proof
149	
150	Yield (%) = (Weight of produced PKO biodiesel/Weight of PKO) $\times$ 100 Eq.1
151	
152	FAME content (%) = $\frac{\text{area of all FAME \times weight of internal standard}}{\text{area of internal standard \times weight of biodiesel sample}} \times 100$ Eq.2
153	
154	Where, FAME content was calculated by GC (Perkin Elmer Claus 580) equipped with a
155	Flame Ionization Detector (FID) and capillary column Select Biodiesel CP9080 (30 m $\times$ 0.32
156	mm $\times$ 0.25 $\mu m)$ and methyl nonadecanoate (C19:0) as the internal standard.
157	
158	2.3. Fuel characterization
159	The density (Hydrometer, accuracy: $\pm 2$ Kg/m <sup>3</sup> ), kinematic viscosity at 40 °C (Red wood
160	viscometer, accuracy: $\pm 0.02 \text{ mm}^2/\text{s}$ ), flash point (Penksy martins apparatus, accuracy: $\pm 2 \text{ °C}$ ),
161	cloud point and pour point (11010-2, Stanhope SETA, accuracy: ±0.5 °C), acid value, iodine
162	value, and Linoleic acid ME content of the PKO biodiesel produced via conventional and
163	microwave heating systems were determined. Further, the chemical components of PKO
164	biodiesel containing fatty acids, free glycerin and total glycerine were also measured by a gas
165	chromatograph (GC) according to recommended ASTM standard method.
166	
167	2.4. Testing the engine performance and exhaust emissions
168	To evaluate the performance of the produced fuels and assess the effect of microwave
169	irradiation on the combustion behavior of PKO biodiesel, the fuels were tested in the diesel
170	engine. A single-cylinder engine equipped with an eddy current dynamometer (WE400) was

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172 1000) was used to measure  $CO_2$ , CO, HC, and  $NO_x$  emissions with its specifications

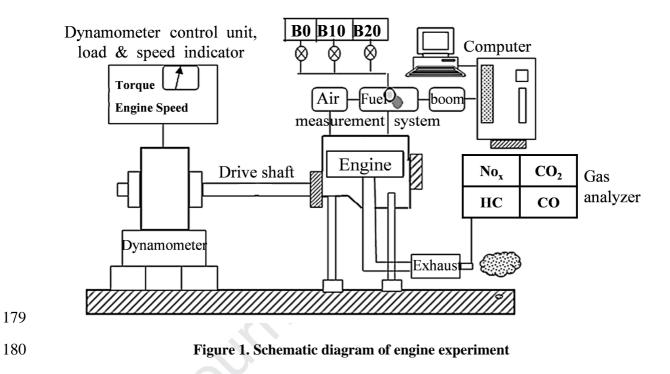
used whose specifications are listed in Table S1. Moreover, an AVL gas analyzer (DIGAS

171

173 summarized in Table S2. Various blends of PKO biodiesel-net diesel fuel (BX where X refers



to volume percentage of biodiesel (x=0, 10, 20 and 40)) were prepared. Then, the engine performance and exhaust gas emissions of the diesel engine fueled by blend fuels were measured. The performance and exhaust gas emissions were evaluated at engine speeds of 1800, 2150, and 2500 rpm at full load. The schematic diagram of the engine experiment is depicted in Figure 1.



181

### 182 **3. Results and discussion**

#### 183 **3.1. Evaluation of palm kernel oil properties**

According to ratio of the weight of the obtained PKO to weight of palm kernels, the palm kernels of Zahidi type had around 10 wt.% oil which can be an appropriate feedstock for biodiesel process. The density of PKO at 25 °C was obtained as 916 kg/m<sup>3</sup>. The PKO revealed a high kinematic viscosity (28 mm<sup>2</sup>/s) causing problem in its flow and spraying in the engine chamber. Therefore, it should been converted to ester (biodiesel) for reducing its viscosity to be used in the engine. Meanwhile, 4.25 wt.% of FFA content (acid value of 8.5 mg KOH/g) of PKO exceeds the limitation for utilization in alkali homogeneous



191 transesterification reaction. Therefore, the esterification reaction with an acid catalyst 192  $(H_2SO_4)$  must have been done to reduce its FFA content. The FFA compositions of PKO are 193 listed in Table 1.

194

#### 195Table 1. FFA compositions of PKO and produced PKO biodiesel by conventional and

196

#### microwave methods

FFA compositions	Unit	РКО	PKO biodiesel	
	Oint	TRO	Conv. <sup>b</sup>	Mic. <sup>c</sup>
Lauric acid (C12:0) <sup>a</sup>	wt.%	21.08	14.8	15.6
Mysteric Acid (C14:0) <sup>a</sup>	wt.%	13.85	9.9	10.4
Palmitic acid (C16:0) <sup>a</sup>	wt.%	12.38	10.8	11.2
Palmitoleic acid (C16:1) <sup>a</sup>	wt.%	$\mathcal{O}$	1.0	1.1
Stearic acid (C18:0) <sup>a</sup>	wt.%	2.73	3.1	3.2
Oleic acid (C18:1) <sup>a</sup>	wt.%	43.23	45.6	46.5
Linoleic acid (C18:2) <sup>a</sup>	wt.%	5.94	11.4	8.8
Other component	wt.%	0.79	3.2	4.3

- <sup>a</sup> Carbon atoms number: double bond number
  - <sup>b</sup> Conv.: Conventional heating system
- <sup>c</sup> Mic.: Microwave heating system
- 200

198

PKO has high unsaturated fatty acid components (58.7 wt.%) with a high unsaturation degree. It contains lauric acid (21.08%), mysteric Acid (13.85%), palmitic acid (12.38%), stearic acid (2.73%), oleic acid (43.23%), and linoleic acid (5.94%). According to the PKO structure, the molecular weight was obtained as 784 g/gmole which was used for measuring the methanol amount for each reaction.

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#### 207 **3.2.** Optimizing the microwave-assisted transesterification reaction parameters

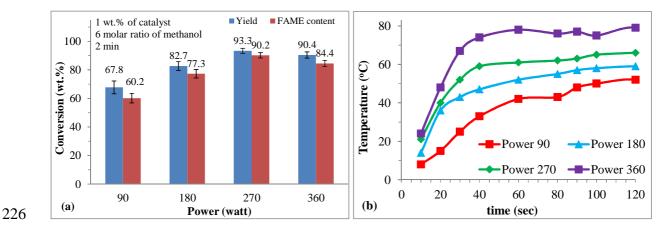
208 3.2.1. Effect of microwave power

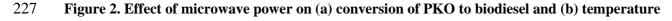
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209 Assessment of the microwave power is very important to obtain the highest yield and the 210 lowest energy consumption. The effect of microwave power is depicted in Figure 2 (a). The 211 yield and FAME content of PKO biodiesel increase by increasing the microwave power from 212 90 W to 270 W due to elevation of the reaction rate. However, the reaction conversion 213 diminished when the microwave power was set at 360 W. It can be related to considerable 214 rise of the reaction temperature medium causing elimination of methanol from liquid to vapor phase. This phenomenon can be proven by detecting the changes in the reaction temperature 215 216 with elevation of microwave power, as shown in Figure 2 (b). An inverse relationship has 217 been observed between the reaction rate enhancement and the boiling point of the solvent in a 218 series of esterification reactions (Jacob et al. 1995).

As seen in the Figure 2 (b), the time of reaching the desirable reaction temperature (around 50 °C) shortened sharply from 80 to 30 sec with the rise of the microwave power from 90 W to 270 W. However, when the microwave power was adjusted on 360 W, the reaction temperature passed the boiling point of methanol (64.7 °C) after 30 sec leading to evaporation of methanol and reduction of its amount in the reaction medium (liquid phase) (Hojjat et al. 2016). Therefore, microwave power of 270 W was selected as optimum for further studies.





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of transesterification reaction

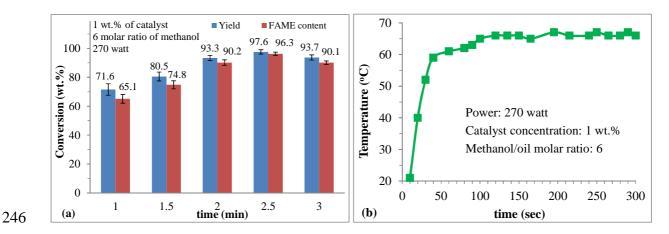


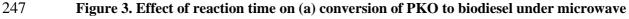
#### 230 *3.2.2. Effect of reaction time*

231 The effect of reaction time on transesterification of PKO was examined at 270 W, 6 molar 232 ratios of methanol/PKO, and 1 wt.% of catalyst with the results illustrated in Figure 3 (a). The conversion rate significantly increased as the time of reaction lengthened from 1 to 2.5 233 234 min, as sufficient time was provided for the interaction between the catalyst and reactants. Further, Figure 3 (b) displays the temperature of microwave-assisted transesterification 235 236 reaction during 5 min. The reaction temperature reached 60 °C after 40 sec. Therefore, more than 40 sec was required for the reaction of the reactants. After 150 sec, the levels of 237 238 conversion decreased slightly due to saponification side reaction (Hojjat et al. 2016). It must 239 be mentioned that the microwave irradiation increased all reactions including saponification reaction. However, since the transesterification is faster than the saponification reaction, 240 methyl esters losses with saponification were negligible at the first moments of reaction. 241 242 However, at longer reaction times, saponification effect has to be taken into account (Casas et 243 al. 2010). Therefore, the equilibrium conversion was almost 97.6% (96.3. % of FAME 244 content) for 150 seconds of reaction time.

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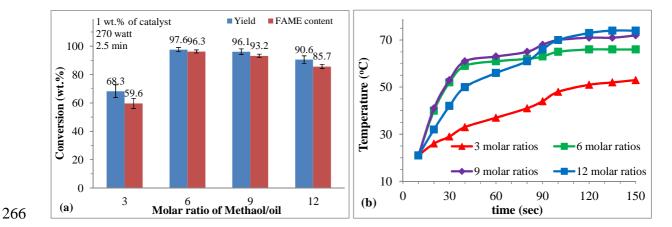
irradiation and (b) temperature of transesterification reaction



268

#### 250 3.2.3. Effect of methanol content

251 In addition to the positive effect of methanol on moving the transesterification reaction 252 forward, methanol can also absorb the microwave irradiation to accelerate the reaction (Hashemzehi et al. 2016). Microwave-assisted transesterification reaction was examined at 253 254 various methanol/oil molar ratios (3, 6, 9, and 12) with the results presented in Figure 4 (a). Expectedly, the conversion increased significantly by raising the the methanol amount. 255 Greater adsorption of microwave irradiation using the reaction medium can be observed 256 257 against the variations of reaction temperature as plotted in Figure 4 (b). It is clearly observed 258 that when the methanol ratio increased from 3 to 6, the final temperature of reaction rose 259 considerably from 53 °C to 66 °C; so did the reaction yield (FAME content) from 68.3% 260 (59.6%) to 97.6% (93.3%). The reaction conversion diminished slightly by using methanolto-oil molar ratio of 9, which can be related to insufficient rise of the reaction temperature, 261 which reduces the methanol amount in the liquid medium (Hashemzehi et al. 2016). In 262 263 addition, due to the high solubility of the by-product (glycerol) and FAME in excessive 264 methanol, the separation becomes difficult and consequently the yield declines (Nayebzadeh 265 et al. 2017).



267 Figure 4. Effect of molar ratio of methanol/oil on (a) conversion of PKO to biodiesel under

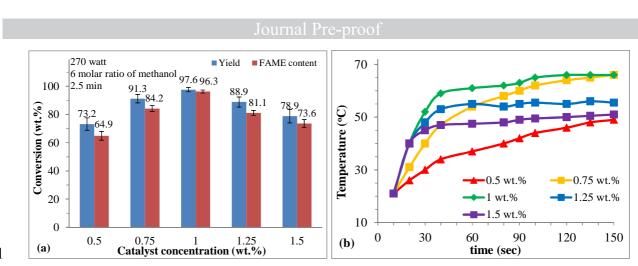
microwave irradiation and (b) temperature of transesterification reaction



#### 270 3.2.4. Effect of catalyst concentration

271 A homogeneous catalyst in the transesterification reaction can have positive and negative 272 effects. The catalyst speeds up a chemical reaction by lowering the amount of activation 273 energy required for the reaction to take place. On the other hand, the base catalyst (NaOH) 274 can react with FFA to form soap which has a negative influence on the yield of transesterification reaction. Therefore, the amount of catalyst must be evaluated with its 275 276 results displayed in Figure 5 (a). The yield increased substantially from 73.2% to 97.6% with 277 elevation of the catalyst loading from 0.5 to 1 wt.%. However, the conversion decreased 278 drastically when higher amounts of the catalyst were introduced into the reaction. Formation 279 of soap affects the viscosity of the reactants whereby the mass transfer occurs with difficulty 280 (Patil et al. 2009).

281 The yield reduction can be also proven by monitoring the changes in transesterification reaction temperature as indicated in Figure 5 (b). It is observed that the rate of temperature 282 283 elevation declines sharply with loading the catalyst to beyond 1 wt.%. Encinar et al. (2012) 284 reported that dielectric constants of the product mixture (methyl ester and glycerol) are 285 greater than those in the reactant (triglycerides and methanol). Soap adsorbs microwave 286 irradiation by starting the saponification reaction, and inhibits the adsorption of microwave 287 irradiation by the reactant or product to elevate the reaction temperature sufficiently. 288 Therefore, the temperature did not grow enough and inappropriate yield was obtained. 289 Accordingly, 1.0 wt.% of catalyst was set as the optimum catalyst amount which is consistent 290 with earlier findings (Liao and Chung 2013, Nayebzadeh et al. 2013).





293

Figure 5. Effect of catalyst concentration on (a) conversion of PKO to biodiesel under microwave irradiation and (b) temperature of transesterification reaction

294

#### 295 **3.3. Biodiesel fuel characteristics and properties**

296 The characterization of fatty acid compositions of the PKO biodiesel produced via conventional and microwave heating systems performed by GC is demonstrated in Table 1. 297 The yield and FAME content of PKO biodiesel produced by conventional method were 298 obtained as 96.4% and 96.3%, respectively. The biodiesel produced by conventional method 299 300 contained 38.6% saturated fatty acids and 58% unsaturated components. On the other hand, 301 the PKO biodiesel produced by microwave method had 40.4% saturated fatty acids and 56.4% unsaturated components with a 65.2% degree of unsaturation. Note that the duration of 302 303 conventional transesterification reaction was 90 min, while the transesterification was 304 completed after 2.5 min under microwave irradiation. The biodiesel produced by microwave 305 irradiation showed lower unsaturation degree that has positive influence on the stability of 306 biodiesel. It can be seen from the content of Linoleic acid ME of biodiesel produced by the both methods. Probably, microwave irradiation can accelerate the reaction between saturated 307 components with alcohol instead of unsaturated components. It well known that microwave 308 309 irradiation can significantly effect on the polar components such as methanol in transesterification reaction. On the other hands, nonpolar lipids are more saturated than polar 310



311 lipids (Nomanbhay and Ong 2017). Therefore, moving a component with the magnetic 312 medium along with fix position a nonpolar component causes to more interaction between 313 them. It can be consequently concluded that, for increasing the reaction between FFAs and 314 methanol, the oils containing more saturated FFAs are more suitable.

315 Oleic acid is the most abundant methyl ester of PKO biodiesel. Further, PKO biodiesel 316 contains around 36% short-chain fatty acids which have a positive effect on its viscosity, 317 cloud point, and pour point.

The physical properties of PKO biodiesel produced by conventional and microwave 318 methods are listed in Table 2. The kinematic viscosity of PKO was reduced from 28 mm<sup>2</sup>/s to 319 4.03 mm<sup>2</sup>/s by transesterification via microwave irradiation which meets the biodiesel 320 standard. However, the kinematic viscosity was reduced to 4.85 mm<sup>2</sup>/s for PKO biodiesel 321 produced by the conventional method. This parameter is important during injection of fuel in 322 323 the diesel engine chamber where lower values are more desirable. Moreover, the density of both PKO biodiesels (microwave and conventional) decreased and obtained as 874 kg/m<sup>3</sup> and 324  $878 \text{ kg/m}^3$ , respectively. 325

The flash point (closed cup) of PKO biodiesel produced by the conventional (107 °C) and 326 microwave transesterification reactions (119 °C) matched the ASTM D6751 (min 93 °C) and 327 328 EN14214 (min 101 °C) standards of biodiesel. Cetane number and calorific value of both fuel 329 are in the limitation range in which the fuel produced by microwave present higher amount. It can be referred to its lower unsaturation degree and higher amount of FAME component with 330 331 longer carbon chain. Moreover, the linoleic acid methyl ester content of microwave and conventional PKO biodiesel was 8.8 wt.% and 11.4 wt.%. which are lower than the amount 332 suggested by EN14214 standard (max 12 wt.%). Both biodiesel present low amount of free 333 334 and total glycerine in their mixture that met the limitation of ASTM and EN standard.



Property	Method	Unit	limit		PKO biodiesel	
riopeny			ASTM D6751	EN 14214	Conv.	Mic.
Density at 15 °C	ASTM D1298	kg/m <sup>3</sup>	-	860-900	878	874
Kinematic viscosity at 40 °C	ASTM D445	mm <sup>2</sup> /s	1.9-6	3.5-5	4.85	4.03
Flash point-closed cup	ASTM D93	°C	93	101	107	119
Cetane number <sup>a</sup>	-	-	48-65	> 51	57.1	57.8
Calorific value <sup>b</sup>	-	MJ/kg	> 35	> 36	41	41.3
Cloud point	-	°C	-	-	6	2
Pour point	-	°C	-		0	-6
Acid value	ASTM D664	mg KOH/g	Max 0.5	Max 0.5	0.25	0.2
Iodine value	EN 14111	gI <sub>2</sub> /100g	-0	Max 120	63	59
Linoleic acid ME	EN14103	wt.%	_	Max 12	11.4	8.8
Free glycerine	ASTM D6584	wt.%	Max 0.02	Max 0.02	0.03	0.02
Total glycerin	ASTM D6584	wt.%	Max 0.24	Max 0.25	0.23	0.021

#### 336 Table 2. Properties of PKO biodiesel produced by conventional and microwave methods

<sup>a</sup> Cetane number calculated by the formula suggested by Gopinath et al. (2009) according to
 biodiesel composition

<sup>b</sup> Calorific value calculated by the formula suggested by Demirbas (2008)

340

#### 341 **3.4.** Effect of biodiesel production method on the engine performance

The blend fuels were labeled as BX-Y concerning the volume of biodiesel in the fuel and the production method, where X is related to volume percentage of biodiesel (0, 10, 20 and 40) and Y is associated to the production method (conventional (Conv.) and microwave (Mic.)).

346

#### 347 *3.4.1. Engine torque and power*

The power and torque of engine fueled by blends of PKO biodiesel produced by the two heating methods with net diesel engine are displayed in Figure 6 and Figure 7, respectively. The power is defined as the rate at which work is done by the engine (Zareh et al. 2017). It

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was previously reported that a lower heating value and higher viscosity of biodiesel compared to net diesel fuel are attributed to diminished engine power. On the other hand, high oxygen content and flammability of biodiesel have a positive influence on the engine power (Miri et al. 2017). The results suggest that the power declines when biodiesel is added to net diesel fuel. However, B40 presents higher brake power compared to other blend fuels at the engine speed of 1800 rpm and 2150 rpm which is related to high oxygen content and flammability of biodiesel.

358 Some researchers believe that higher viscosity of biodiesel enhances fuel spray penetration whereas others reported that the higher viscosity decreases combustion efficiency due to bad 359 360 fuel injection atomization (Damanik et al. 2018). Moreover, it is known that high lubricity of 361 biodiesel might result in the reduced friction loss and thus improve the brake effective power. Therefore, it can be concluded that higher viscosity probably has positive effect such that the 362 fuel produced by conventional method provides higher engine power. Increasing the power 363 by more loading of biodiesel in the blend fuel can confirm the positive effect of viscosity 364 such that the difference between the produced power by net diesel and B40.Mic. is not 365 meaningful. 366

However, at higher engine speeds, although blend fuels presented a higher power 367 368 compared to net diesel fuel, B10 fuels exhibited the maximum power. It is well known that 369 higher amounts of fuel are required at high engine speeds, while blend fuels have a higher density and viscosity, affecting the fuel injection system. Therefore, B40 fuel leads to more 370 371 injection problem where the power declines at higher engine speeds (Hoseini et al. 2017). Although a higher power was obtained at the maximum engine speeds such that the 372 maximum power of 4.54 kW and 4.45 kW was obtained for B10-Conv. and B10.Mic. 373 374 respectively, B40 can be a suitable choice for low engine speeds.

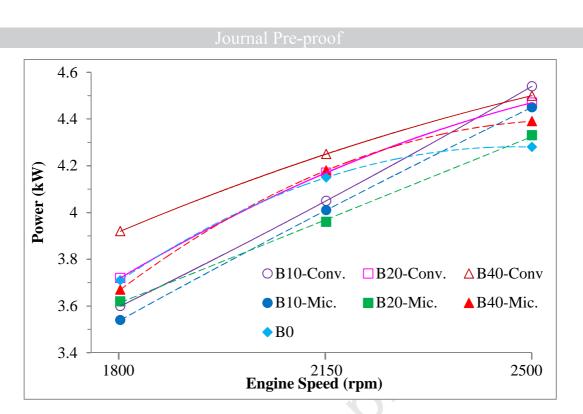
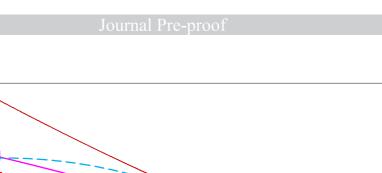


Figure 6. Effect of heating system used for biodiesel production process on the power of engine
 fueled by various diesel-biodiesel blends worked at different engine speeds

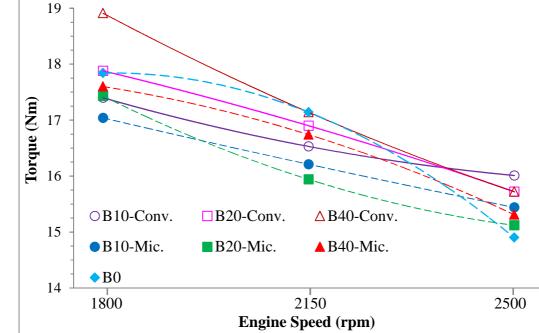
379

380 Since the produced power is directly proportional to the torque, the same trend as of power 381 was observed for torque as well. The torque will decrease with elevation of engine speed and 382 adding the biodiesel to fuel because of reducing the force on the piston and crankshaft and 383 low heating value of the biodiesel, respectively (Noorollahi et al. 2018). Although low 384 heating value of biodiesel negatively affects the engine ignition and reduces engine torque, 385 biodiesel improves the lubricity of diesel fuel thereby reducing the friction loss and thus improving the effective torque (as can be seen for B40.Conv. at 1800 rpm). This grows for 386 387 the fuels at the maximum engine speed (2500 rpm) in which higher torque is obtained because of higher injection of fuel to chamber, and increasing the lubricity and oxygen 388 389 content of medium (Zaharin et al. 2017).

The difference in the torque provided by biodiesel produced by different method may be referred to higher viscosity of those produced by conventional method that leads to more injection of fuel in the engine camber, especially at higher engine speed (Zaharin et al. 2017).









395 Figure 7. Effect of heating system used for biodiesel production process on the torque of engine 396 fueled by various diesel-biodiesel blends worked at different engine speeds

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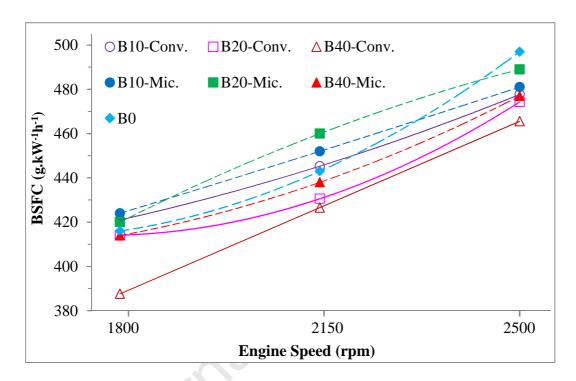
398 3.4.2. Brake-Specific fuel consumption

399 The influence of blending the diesel fuel with PKO biodiesel, biodiesel production 400 method, and engine speed on the Brake-specific fuel consumption (BSFC) is illustrated in 401 Figure 8. The volume of injected fuel, fuel density, viscosity, and heating value of fuel affect 402 the BSFC of diesel engine defined as the mass fuel flow rate to the brake power ratio 403 (Ozsezen et al. 2009). BSCF increases by adding PKO biodiesel at low engine speeds due to 404 lower heating and calorific values of blends fuel compared with net diesel fuel that causes to 405 more amount of blends are required to produce the same amount of engine power output by 406 the engine (Zaharin et al. 2017, Rajak and Verma 2018). In addition, the proper atomization 407 of the fuel is probably prevented by the high viscosity of the blends, which in turn affects the 408 combustion process (Soukht Saraee et al. 2017) However, the BSFC declines with further 409 loading of biodiesel in the diesel fuel due to elevation of the oxygen content of the medium



410 and better combustion of the fuel (Lin and Lin 2006). This behavior can be proved with the 411 rise of the brake power at high engine speeds. Across the entire engine speeds, B40 fuel 412 presented the lowest SCF for the both produced biodiesel due to its lower viscosity, probably.

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Figure 8. Effect of heating system used for biodiesel production process on BSFC of engine
 fueled by various diesel-biodiesel blends worked at different engine speeds

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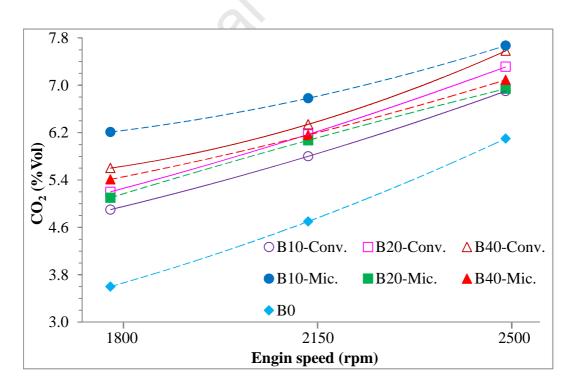
#### 418 **3.5. Emission analysis**

#### 419 *3.5.1. CO*<sub>2</sub> *emissions*

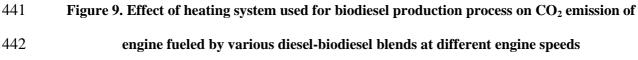
420  $CO_2$  emissions in the exhaust gas of the diesel engine fueled by different blend fuels and 421 operating at various engine speeds are presented in Figure 9. It is expected for biodiesel-422 diesel fuel to release higher amounts of  $CO_2$  due to the higher oxygen content of biodiesel 423 compared to diesel fuel (Yusaf et al. 2011, Bayındır et al. 2017). However, it was observed 424 that by increasing the ratio of PKO biodiesel produced by conventional method to the net 425 diesel fuel, the amount of  $CO_2$  in the emission gas rose, while this behavior was not observed 426 for that produced by microwave irradiation.

427 This can be attributed to two reasons. Microwave-assisted produced PKO biodiesel has a 428 lower viscosity and density which inhibits the high amount of fuel injection in the chamber, 429 where lower amounts of CO<sub>2</sub> were released as compared to use of conventional produced 430 PKO biodiesel. On the other hand, the higher flash point of PKO biodiesel produced by 431 microwave irradiation probably accelerates other side reactions of carbon combustion leading 432 to less CO<sub>2</sub> formation. Assessment of the other emissions in exhaust gas can determine the main reason for this behavior. On the other hands, it was pointed in the case of biodiesel 433 434 emissions that the higher carbon dioxide emission should cause less concern because of 435 Nature's recovery by raising biodiesel crops (Rajaeifar et al. 2014, Nguyen et al. 2017). The life cycle of CO<sub>2</sub> emissions of biodiesel revealed that biodiesel will cause 50-80% reduction 436 437 in CO<sub>2</sub> emissions compared to petroleum diesel (Qi et al. 2010, Jørgensen et al. 2012, Esteves 438 et al. 2017).

439



440





444 *3.5.2. CO emissions* 

445 The amount of CO released by different fuels at various engine speeds is depicted in 446 Figure 10. When incomplete combustion or progression from CO to CO<sub>2</sub> occurs in the engine 447 chamber, higher amounts of CO form in the exhaust gas emission. The results suggest that CO emission declines using blend fuels. This can be related to higher oxygen contents of fuel 448 449 because of more complete combustion of fuel, which is consistent with the results of CO<sub>2</sub> content in the exhaust emission (Song and Zhang 2008, Gharehghani et al. 2019). Therefore, 450 451 a significant reduction in the CO content with enlargement of the biodiesel volume in blends is acceptable with B20-Mic. and B40.Mic. presenting the lowest CO emissions at all engine 452 453 speeds. Moreover, B40-Conv. also exhibited better fuel combustion in the engine chamber 454 where the lowest CO was detected. The reduction in the CO content in the exhaust by raising 455 the engine speed is a result of the better air-fuel mixing process and/or the increased fuel/air 456 equivalence ratio (Pinto et al. 2005).

The PKO biodiesel produced by microwave irradiation showed more sufficient combustion compared to that prepared by the conventional method where very low CO emission was detected in the exhaust gas. It was mentioned that CO emissions reduced much higher with the increasing of chain length (Knothe et al. 2006). The biodiesel produced by microwave presented higher amount of all of FFA components, except of Linoleic acid ME, that effect on the well combustion of fuel in the engine chamber.

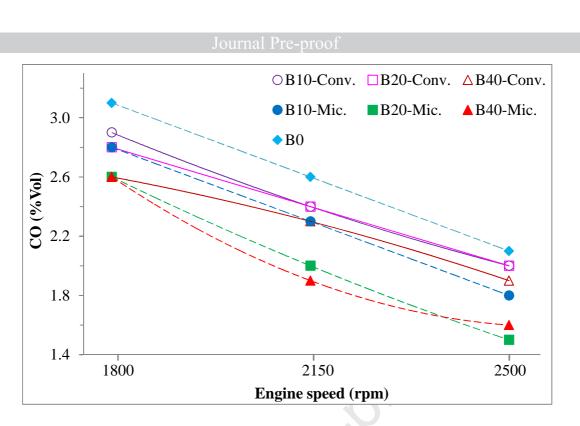


Figure 10. Effect of heating system used for biodiesel production process on CO emission of
 engine fueled by various diesel-biodiesel blends at different engine speeds

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#### 468 *3.5.3. HC emissions*

Figure 7 displays the effect of increasing the biodiesel to net diesel fuel ratio on the HC emission of the engine diesel working at various engine speeds and full load. It was described that the combustion of fuels in the engine chamber improves by blending the diesel fuel with biodiesel. Therefore, it is expected that the amount of unreacted hydrocarbon (HC) decreases. Furthermore, shortening the burning delay using biodiesel blends results in diminished HC emissions due to its higher cetane number (Yusaf et al. 2011, Soukht Saraee et al. 2017).

475 Note that PKO biodiesel produced by microwave irradiation exhibits a better behavior in 476 the combustion of hydrocarbons into the engine chamber, which can be related to its lower 477 density as well as viscosity and higher cetane number (Kumar et al. 2009, Sharma et al. 478 2019). Moreover, increase in chain length and saturation level of biodiesel leads to a higher 479 reduction in HC emission (Knothe et al. 2006). The biodiesel produced by microwave



480 irradiation exhibit higher amount of ester with longer chain length and lower unsaturation481 degree that improves its combustion in the engine chamber.

482 Due to the high viscosity of PKO biodiesel produced by conventional method, high 483 amounts of fuel were injected into the chamber causing incomplete fuel combustion. 484 Therefore, higher CO and HC levels were released which is in good agreement with CO<sub>2</sub> 485 results. Therefore, microwave-assisted produced PKO biodiesel is the best fuel for blending 486 with biodiesel for more complete combustion of carbon groups in the engine chamber, with 487 B40 presenting a great ability for mixing with net diesel fuel.



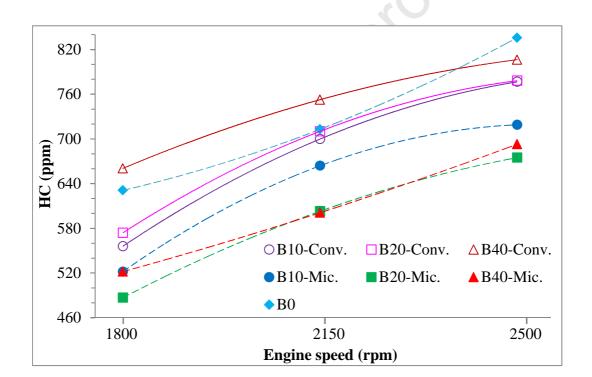




Figure 11. Effect of heating system used for biodiesel production process on HC emission of
 engine fueled by various diesel-biodiesel blends at different engine speeds

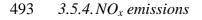


Figure 12 reveals the variations of  $NO_x$  emission with engine speed by running diesel engine with different fuel blends. Higher  $NO_x$  emissions occur in the exhaust using blend fuels due to the higher flash point and oxygen content of biodiesel, resulting in augmented



497 gas temperature in the engine chamber and accelerated interaction between oxygen and 498 nitrogen (Xue et al. 2011). Faster premixed combustion by addition of the biodiesel to diesel 499 fuel leads to elevated combustion temperature to over 1800 K causing NOx formation 500 (Zaharin et al. 2017, Sharma et al. 2019). B20-Mic. and B10-Conv. showed the lowest  $NO_x$ 501 content in the exhaust, though B40-Mic. presented a similar  $NO_x$  amount in the exhaust gases 502 at high engine speeds.

Further, the  $NO_x$  emission diminished continuously with elevation of the engine speed. It can be related to the shorter residence time available for NOx formation, which may be owing to the rise in both the volumetric efficiency and flow velocity of the reactant mixture at higher engine speeds (Lin and Lin 2006). The minimum increase in the  $NO_x$  content was observed for B20-Mic. at the engine speed of 1800 rpm which is consistent with the results of other studies (Lin et al. 2008, Hoseini et al. 2017). Finally, B40-Mic. and B20-Mic. provided almost similar  $NO_x$  emissions at the other engine speeds.

It was mentioned that a less increase in NOx emission can be observed by using the 510 511 biodiesel containing the more saturated carbon bonds (Lin et al. 2009, Sharma et al. 2019). It 512 can prove the similarity of NOx emission when blend of diesel-biodiesel produced by microwave irradiation was utilized. In the other words, NOx emissions increase by raising the 513 514 degree of unsaturation of biodiesel (increase the unsaturated components) (Lin and Lin 515 2006). Moreover, advance in combustion for biodiesel due to shortens ignition delay, and 516 advance of start of injection of biodiesel due to the higher density and viscosity are the 517 reasons for higher NOx of fuel blended with biodiesel produced by conventional method.

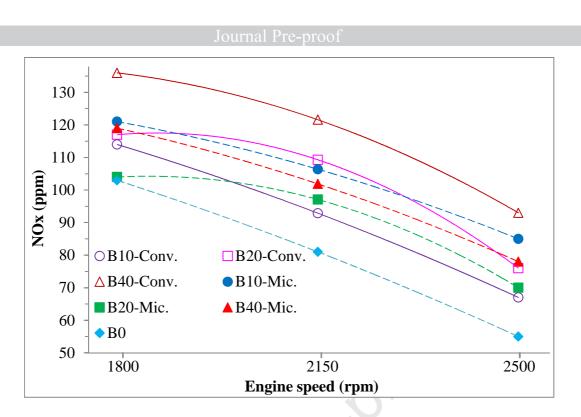


Figure 12. Effect of heating system used for biodiesel production process on NO<sub>x</sub> emission of
 engine fueled by various diesel-biodiesel blends at different engine speeds

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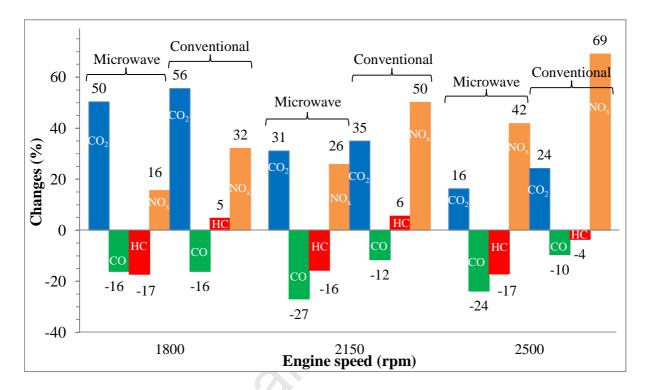
#### 522 3.5.5. Comparison the emissions of B40

After chosen B40 as a suitable proposition for blending the biodiesel with diesel fuel, the 523 CO<sub>2</sub>, CO, HC and NOx emission contents were summarized in Figure 13. It clearly observes 524 525 that the fuel produced by microwave irradiation exhibits better emissions profile in all of 526 engine speeds. Lower increasing in the amount of NOx and CO<sub>2</sub> along with higher reduction 527 of CO and HC prove that microwave irradiation changes the properties of produced biodiesel 528 by effecting on the kind of FFA components. Probably under microwave medium, the 529 nonpolar components (saturated FFA) easily react with polar component (methanol as 530 alcohol) to form ester. It causes to saturation components form more than unsaturation 531 components that lead to reduction the unsaturation degree and better combustion of fuel in 532 the engine chamber, as mentioned above. Therefore, the microwave irradiation can concern 533 as an effective method for fabrication of a same biodiesel fuel with low unsaturated



534 components that significantly decreases the emissions released from those produced by

- 535 conventional method.
- 536



537

Figure 13. Comparison the emissions of B40 fuels produced by conventional and microwave
 heating systems fueled in diesel engine at different engine speeds

540

#### 541 **4.** Conclusion

542 Palm kernel oil (PKO) contains appropriate amounts of oil making it a suitable source for 543 biodiesel production. Accordingly, its performance in the diesel engine was firstly compared 544 when microwave and conventional heating systems were utilized for converting PKO to biodiesel. The palm seed (Zahidi type) contained 10 wt.% oil in which a high FFA content 545 546 was observed. After reducing the FFA content of PKO via esterification reaction, the PKO 547 was transesterified via conventional and microwave irradiation heating systems with methanol and NaOH as a catalyst. A biodiesel yield of 96.4% was obtained at the conditions 548 of 60 °C, methanol/PKO molar ratio of 6, 1 wt.% catalyst, and 90 min of the reaction time for 549

550 conventional method. On the other hand, microwave irradiation reduced the reaction time to 551 2.5 min and enhanced the yield to 97.6%. In addition to shortening the reaction time, the separation step was also curtailed from 4 h to 4 min using microwave irradiation. Both PKO 552 553 biodiesels produced by conventional and microwave method met the ASTM D6751 and EN14214 standard specifications. The temperature monitoring of microwave-assisted 554 555 transesterification reaction showed that the reaction temperature must be lower than the boiling point of the utilized alcohol to achieve the maximum conversion. Assessment of the 556 557 performance and exhaust gas emissions of a single-cylinder engine fueled by blends of PKO biodiesel-diesel suggested that PKO biodiesel produced by the conventional method 558 559 presented a higher brake power and torque and lower BSFC compared to that prepared by the 560 microwave method. All fuels revealed a higher power and torque at the engine speed of 2500 561 rpm as compared to engine speeds of 1800 rpm and 2150 rpm.

Overall, B40 (both PKO biodiesels produced by different heating systems) can be a choice 562 for improvement the problems of net diesel fuel by blending with biodiesel in which the 563 564 biodiesel has higher proportion compared to commercial blend fuel (B20). The exhaust gas emissions analysis suggested that PKO biodiesel exhibited reduction in CO and HC 565 emissions in exhaust due to elevation of oxygen content of the fuel leading to better 566 567 combustion. On the other hands, increase of CO<sub>2</sub> and NOx contents was observed by using biodiesel. Unlike the results of engine performance, PKO biodiesel produced by microwave 568 569 irradiation showed better results in releasing the emissions which can be related to its lower 570 density and viscosity. These properties mitigate the problem of fuel injection in the engine chamber. B40 also presented appropriate properties in the analysis of the emissions. The 571 results confirmed that PKO biodiesel has very suitable properties which can be blended with 572 573 net diesel fuel at a higher volume ratio (B40). Moreover, microwave irradiation, by shortening the transesterification time, improving the properties of produced biodiesel, and 574



significantly reducing the exhaust gas emissions, can be regarded as an alternative method for

industrial biodiesel production to reduce greenhouse gas problems.
It must be mentioned that the FFAs compositions of PKO is strongly depends on the
climate as well as engine performance that would be some limitations. Moreover, this study
must be developed on assessment the engine load, broder engine speed, different engine type
(containing more cylinder) that will be presented in our future work.

581

575

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586

### 587 **Declarations of interest**

588 None

589

#### 590 **Reference**

591

Abdul Kapor, N.Z., Maniam, G.P., Rahim, M.H.A., Yusoff, M.M., 2017. Palm fatty acid
distillate as a potential source for biodiesel production-a review. Journal of Cleaner
Production 143, 1-9.

595 Aladetuyi, A., Olatunji, G.A., Ogunniyi, D.S., Odetoye, T.E., Oguntoye, S.O., 2014.

- 596 Production and characterization of biodiesel using palm kernel oil; fresh and recovered
- from spent bleaching earth Biofuel Research Journal 1, 134-138.



- Alamu, O.J., Waheed, M.A., Jekayinfa, S.O., Akintola, T.A., 2007. Optimal
  Transesterification Duration for Biodiesel Production from Nigerian Palm Kernel Oil
  Agricultural Engineering International: the CIGR journal. IX, 1-11.
- Ali, M.A., Al-Hattab, T.A., Al-Hydary, I.A., 2015. Extraction of date palm seed oil (*phoenix dactylifera*) by soxhlet apparatus. International Journal of Advances in Engineering &
- 603 Technology 8, 261-271.
- Aranda, D.G., Santos, R.P., Tapanes, N.O., Ramos, A., Antunes, O., 2008. Acid-Catalyzed
  Homogeneous Esterification Reaction for Biodiesel Production from Palm Fatty Acids.
  Catalysis Letters 122, 20-25.
- Bautista, S., Espinoza, A., Narvaez, P., Camargo, M., Morel, L., 2019. A system dynamics
  approach for sustainability assessment of biodiesel production in Colombia. Baseline
  simulation. Journal of Cleaner Production 213, 1-20.
- Bayındır, H., Işık, M.Z., Argunhan, Z., Yücel, H.L., Aydın, H., 2017. Combustion,
  performance and emissions of a diesel power generator fueled with biodiesel-kerosene
  and biodiesel-kerosene-diesel blends. Energy 123, 241-251.
- 613 Bello, E.I., Oguntuase, B., Osasona, A., Mohammed, T.I., 2015. Characterization and Engine
- 614 Testing of Palm Kernel Oil Biodiesel. European Journal of Engineering and
  615 Technology 3, 1-14.
- Benjapornkulaphong, S., Ngamcharussrivichai, C., Bunyakiat, K., 2009. Al<sub>2</sub>O<sub>3</sub>-supported
  alkali and alkali earth metal oxides for transesterification of palm kernel oil and
- 618 coconut oil. Chemical Engineering Journal 145, 468-474.
- Casas, A., Fernández, C.M., Ramos, M.J., Pérez, Á., Rodríguez, J.F., 2010. Optimization of
  the reaction parameters for fast pseudo single-phase transesterification of sunflower oil.
  Fuel 89, 650-658.

- 622 Chuah, L.F., Klemeš, J.J., Yusup, S., Bokhari, A., Akbar, M.M., 2017. A review of cleaner
- 623 intensification technologies in biodiesel production. Journal of Cleaner Production 146,624 181-193.
- 625 Damanik, N., Ong, H.C., Tong, C.W., Mahlia, T.M.I., Silitonga, A.S., 2018. A review on the
- engine performance and exhaust emission characteristics of diesel engines fueled with
- biodiesel blends. Environmental Science and Pollution Research 25, 15307-15325.
- Demirbas, A., 2008. Relationships derived from physical properties of vegetable oil and
  biodiesel fuels. Fuel 87, 1743-1748.
- Encinar, J.M., González, J.F., Martínez, G., Sánchez, N., Pardal, A., 2012. Soybean oil
  transesterification by the use of a microwave flow system. Fuel 95, 386-393.
- Esteves, V.P.P., Esteves, E.M.M., Bungenstab, D.J., Feijó, G.L.D., Araújo, O.d.Q.F.,
  Morgado, C.d.R.V., 2017. Assessment of greenhouse gases (GHG) emissions from the
  tallow biodiesel production chain including land use change (LUC). Journal of Cleaner
  Production 151, 578-591.
- Fazal, M.A., Suhaila, N.R., Haseeb, A.S.M.A., Rubaiee, S., Al-Zahrani, A., 2018. Influence
  of copper on the instability and corrosiveness of palm biodiesel and its blends: An
  assessment on biodiesel sustainability. Journal of Cleaner Production 171, 1407-1414.
- García-Martínez, N., Andreo-Martínez, P., Quesada-Medina, J., de los Ríos, A.P., Chica, A.,
  Beneito-Ruiz, R., Carratalá-Abril, J., 2017. Optimization of non-catalytic
  transesterification of tobacco (Nicotiana tabacum) seed oil using supercritical methanol
- to biodiesel production. Energy Conversion and Management 131, 99-108.
- Gharehghani, A., Asiaei, S., Khalife, E., Najafi, B., Tabatabaei, M., 2019. Simultaneous
  reduction of CO and NOx emissions as well as fuel consumption by using water and
  nano particles in Diesel–Biodiesel blend. Journal of Cleaner Production 210, 11641170.



- Gopinath, A., Puhan, S., Nagarajan, G., 2009. Relating the cetane number of biodiesel fuels
  to their fatty acid composition: A critical study. Proceedings of the Institution of
  Mechanical Engineers, Part D: Journal of Automobile Engineering 223, 565-583.
- Hashemzehi, M., Saghatoleslami, N., Nayebzadeh, H., 2016. Microwave-assisted solution
  Combustion Synthesis of Spinel-type mixed Oxides for Esterification Reaction.
  Chemical Engineering Communications 204, 415-423.
- Hashemzehi, M., Saghatoleslami, N., Nayebzadeh, H., 2016. A study on the structure and catalytic performance of  $Zn_xCu_{1-x}Al_2O_4$  catalysts synthesized by the solution combustion method for the esterification reaction. Comptes Rendus Chimie 19, 955-962.
- Hayyan, A., Alam, M.Z., Mirghani, M.E.S., Kabbashi, N.A., Hakimi, N.I.N.M., Siran, Y.M.,
  Tahiruddin, S., 2010. Sludge palm oil as a renewable raw material for biodiesel
  production by two-step processes. Bioresource Technology 101, 7804-7811.
- Hojjat, M., Nayebzadeh, H., Khadangi-Mahrood, M., Rahmani-Vahid, B., 2016.
  Optimization of process conditions for biodiesel production over CaO–Al<sub>2</sub>O<sub>3</sub>/ZrO<sub>2</sub>
  catalyst using response surface methodology. Chemical Papers 71, 689-698.
- 663 Hoseini, S.S., Najafi, G., Ghobadian, B., Rahimi, A., Yusaf, T., Mamat, R., Sidik, N.A.C.,
- Azmi, W.H., 2017. Effects of biodiesel fuel obtained from Salvia macrosiphon oil
  (ultrasonic-assisted) on performance and emissions of diesel engine. Energy 131, 289296.
- Igbokwe, J.O., Nwafor, O.M.I., 2016. Performance characteristics of palm kernel biodiesel
  and its blend in a CI engine. International Journal of Ambient Energy 37, 103-106.
- 669 Igbokwe, J.O., Nwufo, O.C., Nwaiwu, C.F., 2015. Effects of blend on the properties,
- 670 performance and emission of palm kernel oil biodiesel. Biofuels 6, 1-8.



- Jacob, J., Chia, L.H.L., Boey, F.Y.C., 1995. Thermal and non-thermal interaction of
  microwave radiation with materials. Journal of Materials Science 30, 5321-5327.
- Jamil, F., Saxena, S.K., Al-Muhtaseb, A.a.H., Baawain, M., Al-Abri, M., Viswanadham, N.,
- Kumar, G., Abu-Jrai, A.M., 2017. Valorization of waste "date seeds" bio-glycerol for
  synthesizing oxidative green fuel additive. Journal of Cleaner Production 165, 10901096.
- 577 Jitputti, J., Kitiyanan, B., Rangsunvigit, P., Bunyakiat, K., Attanatho, L., Jenvanitpanjakul,
- P., 2006. Transesterification of crude palm kernel oil and crude coconut oil by different
  solid catalysts. Chemical Engineering Journal 116, 61-66.
- Jørgensen, A., Bikker, P., Herrmann, I.T., 2012. Assessing the greenhouse gas emissions
  from poultry fat biodiesel. Journal of Cleaner Production 24, 85-91.
- Knothe, G., Sharp, C.A., Ryan, T.W., 2006. Exhaust Emissions of Biodiesel, Petrodiesel,
  Neat Methyl Esters, and Alkanes in a New Technology Engine. Energy & Fuels 20,
  403-408.
- Kumar, M.S., Ramesh, A., Nagalingam, B., 2009. A Comparison of the Different Methods of
  Using Jatropha Oil as Fuel in a Compression Ignition Engine. Journal of Engineering
  for Gas Turbines and Power 132, 032801-032801-032810.
- Liao, C.-C., Chung, T.-W., 2013. Optimization of process conditions using response surface
  methodology for the microwave-assisted transesterification of Jatropha oil with KOH
  impregnated CaO as catalyst. Chemical Engineering Research and Design 91, 24572464.
- Lin, B.-F., Huang, J.-H., Huang, D.-Y., 2008. Effects of Biodiesel from Palm Kernel Oil on
  the Engine Performance, Exhaust Emissions, and Combustion Characteristics of a
  Direct Injection Diesel Engine. Energy & Fuels 22, 4229-4234.



- Lin, B.-F., Huang, J.-H., Huang, D.-Y., 2009. Experimental study of the effects of vegetable
  oil methyl ester on DI diesel engine performance characteristics and pollutant
  emissions. Fuel 88, 1779-1785.
- Lin, C.-Y., Lin, H.-A., 2006. Diesel engine performance and emission characteristics of
  biodiesel produced by the peroxidation process. Fuel 85, 298-305.
- Lubes, Z.I.Z., Zakaria, M., 2009. Analysis of parameters for fatty acid methyl esters
   production from refined palm oil for use as biodiesel in the single- and two- stage
   processes. Malaysian Journal of Biochemistry and Molecular Biology 17, 5-9.
- 703 Mahmudul, H.M., Hagos, F.Y., Mamat, R., Adam, A.A., Ishak, W.F.W., Alenezi, R., 2017.
- Production, characterization and performance of biodiesel as an alternative fuel in
   diesel engines A review. Renewable and Sustainable Energy Reviews 72, 497-509.
- Miri, S.M.R., Mousavi Seyedi, S.R., Ghobadian, B., 2017. Effects of biodiesel fuel
  synthesized from non-edible rapeseed oil on performance and emission variables of
  diesel engines. Journal of Cleaner Production 142, 3798-3808.
- Nayebzadeh, H., Saghatoleslami, N., Rahmani Vahid, B., Maskooki, A., 2013. Effect of
  calcination temperature on catalytic activity of synthesis SrO/S-ZrO<sub>2</sub> by solvent-free
  method in esterification of oleic acid. Chemical and Biochemical Engineering Quarterly
  23, 267-273.
- Nayebzadeh, H., Saghatoleslami, N., Tabasizadeh, M., 2017. Application of Microwave
  Irradiation for Preparation of a KOH/Calcium Aluminate Nanocatalyst and Biodiesel.
  Chemical Engineering & Technology 40, 1826-1834.
- Ngamcharussrivichai, C., Totarat, P., Bunyakiat, K., 2008. Ca and Zn mixed oxide as a
  heterogeneous base catalyst for transesterification of palm kernel oil. Applied Catalysis
  A: General 341, 77-85.



- 719 Ngamcharussrivichai, C., Wiwatnimit, W., Wangnoi, S., 2007. Modified dolomites as 720 catalysts for palm kernel oil transesterification. Journal of Molecular Catalysis A: 721 Chemical 276, 24-33. Nguyen, T.A., Kuroda, K., Otsuka, K., 2017. Inclusive impact assessment for the 722 sustainability of vegetable oil-based biodiesel - Part I: Linkage between inclusive 723 724 impact index and life cycle sustainability assessment. Journal of Cleaner Production 725 166, 1415-1427. Nomanbhay, S., Ong, M.Y., 2017. A Review of Microwave-Assisted Reactions for Biodiesel 726 727 Production. Bioengineering 4, 57-78. 728 Noorollahi, Y., Azadbakht, M., Ghobadian, B., 2018. The effect of different diesterol (diesel-729 biodiesel-ethanol) blends on small air-cooled diesel engine performance and its exhaust 730 gases. Energy 142, 196-200. 731 Ojolo, S.J., Adelaja, A.O., Sobamowo, G.M., 2012. Production of Bio-Diesel from Palm Kernel Oil and Groundnut Oil. Advanced Materials Research 367, 501-506. 732 733 Ong, H.C., Milano, J., Silitonga, A.S., Hassan, M.H., Shamsuddin, A.H., Wang, C.-T., Indra 734 Mahlia, T.M., Siswantoro, J., Kusumo, F., Sutrisno, J., 2019. Biodiesel production from
- Calophyllum inophyllum-Ceiba pentandra oil mixture: Optimization and
  characterization. Journal of Cleaner Production 219, 183-198.
- Ozsezen, A.N., Canakci, M., Turkcan, A., Sayin, C., 2009. Performance and combustion
  characteristics of a DI diesel engine fueled with waste palm oil and canola oil methyl
  esters. Fuel 88, 629-636.
- 740 Patil, P.D., Gude, V.G., Camacho, L.M., Deng, S., 2009. Microwave-Assisted Catalytic
- 741 Transesterification of Camelina Sativa Oil. Energy & Fuels 24, 1298-1304.



- 742 Phoon, L.Y., Mustaffa, A.A., Hashim, H., Mat, R., Manan, Z.A., Yunus, N.A., 2017.
- Performance and emission characteristics of green diesel blends containing diethylsuccinate and 1-octanol. Journal of Cleaner Production 161, 1192-1202.
- 745 Pinto, A.C., Guarieiro, L.L.N., Rezende, M.J.C., Ribeiro, N.M., Torres, E.A., Lopes, W.A.,
- Pereira, P.A.d.P., Andrade, J.B.d., 2005. Biodiesel: an overview. Journal of the
  Brazilian Chemical Society 16, 1313-1330.
- Qi, D.H., Chen, H., Geng, L.M., Bian, Y.Z., 2010. Experimental studies on the combustion
  characteristics and performance of a direct injection engine fueled with biodiesel/diesel
  blends. Energy Conversion and Management 51, 2985-2992.
- Quirino, M.R., Oliveira, M.J.C., Keyson, D., Lucena, G.L., Oliveira, J.B.L., Gama, L., 2016.
  Synthesis of zinc aluminate with high surface area by microwave hydrothermal method
  applied in the transesterification of soybean oil (biodiesel). Materials Research Bulletin
  754 74, 124-128.
- Rajaeifar, M.A., Ghobadian, B., Safa, M., Heidari, M.D., 2014. Energy life-cycle assessment
  and CO2 emissions analysis of soybean-based biodiesel: a case study. Journal of
  Cleaner Production 66, 233-241.
- Rajak, U., Verma, T.N., 2018. Spirulina microalgae biodiesel A novel renewable alternative
  energy source for compression ignition engine. Journal of Cleaner Production 201, 343357.
- Rupilius, W., Ahmad, S., 2007. Palm oil and palm kernel oil as raw materials for basic
  oleochemicals and biodiesel. European Journal of Lipid Science and Technology 109,
  433-439.
- Sharma, V., Duraisamy, G., Cho, H.M., Arumugam, K., Alosius M, A., 2019. Production,
  Combustion and Emission Impact of Bio-mix Methyl Ester Fuel on a Stationary Light
  Duty Diesel Engine. Journal of Cleaner Production.



767

Shote, A.S., Betiku, E., Asere, A.A., 2019. Characteristics of CO and NOx emissions from

768 combustion of transmethylated palm kernel oil-based biodiesel blends in a compression ignition engine. Journal of King Saud University - Engineering Sciences 31, 178-183. 769 770 Song, J.-T., Zhang, C.-H., 2008. An experimental study on the performance and exhaust emissions of a diesel engine fuelled with soybean oil methyl ester. Proceedings of the 771 772 Institution of Mechanical Engineers, Part D: Journal of Automobile Engineering 222, 2487-2496. 773 Soukht Saraee, H., Jafarmadar, S., Sayadi, M., Parikhani, A., Kheyrollahi, J., Pourvosoughi, 774 N., 2017. Green fuel production from Pistacia Khinjuk and its engine test analysis as a 775 776 promising alternative. Journal of Cleaner Production 156, 106-113. 777 Xie, Q., Cai, L., Xia, F., Liang, X., Wu, Z., Liu, Y., Li, X., Lu, M., Nie, Y., Ji, J., 2019. High vacuum distillation for low-sulfur biodiesel production: From laboratory to large scale. 778 779 Journal of Cleaner Production 223, 379-385. 780 Xue, J., Grift, T.E., Hansen, A.C., 2011. Effect of biodiesel on engine performances and 781 emissions. Renewable and Sustainable Energy Reviews 15, 1098-1116. Yusaf, T.F., Yousif, B.F., Elawad, M.M., 2011. Crude palm oil fuel for diesel-engines: 782 Experimental and ANN simulation approaches. Energy 36, 4871-4878. 783 784 Zaharin, M.S.M., Abdullah, N.R., Najafi, G., Sharudin, H., Yusaf, T., 2017. Effects of 785 physicochemical properties of biodiesel fuel blends with alcohol on diesel engine performance and exhaust emissions: A review. Renewable and Sustainable Energy 786 787 Reviews 79, 475-493. Zareh, P., Zare, A.A., Ghobadian, B., 2017. Comparative assessment of performance and 788 emission characteristics of castor, coconut and waste cooking based biodiesel as fuel in 789 790 a diesel engine. Energy 139, 883-894.

Zullaikah, S., Lai, C.-C., Vali, S.R., Ju, Y.-H., 2005. A two-step acid-catalyzed process for
the production of biodiesel from rice bran oil. Bioresource Technology 96, 1889-1896.

793

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# Precise Evaluation the Effect of Microwave Irradiation on the Properties of Palm Kernel Oil Biodiesel Used in a Diesel Engine

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#### **Research Highlights**

- Biodiesel production from palm kernel oil using conventional and microwave methods
- Optimization of transesterification reaction conditions under microwave irradiation
- Assessment the variations of reaction temperature by changing each parameter
- Evaluation the performance and emissions of a diesel engine fuelled by blend fuels
- Finding B40-Mic. and B40-Conv. fuels for using in the diesel engine.

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